Drainage Reports Abbreveated Water & Sewer Need Reports Water Study

Wastewater Study
Stormwater Waiver Application

Preliminary

Drainage Report

Deer Valley Townhomes

NWC Miller Rd & Deer Valley

City of Scottsdale

Maricopa County, Arizona

TSC Project No. 0800

August 27, 2018

Prepared for:

Beardsley 22, Inc.

222 W Linger Lane

Phoenix, AZ 85021



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Preliminary

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Deer Valley Townhomes

NWC Miller Rd & Deer Valley

City of Scottsdale

Maricopa County, Arizona

TSC Project No. 0800

July 18, 2018

Prepared for:

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222 W Linger Lane

Phoenix, AZ 85021



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1.0 Introduction

1.1 Report Purpose

The purpose of this preliminary drainage report is to provide hydrologic and hydraulic documentation for the proposed Deer Valley Townhomes site. More specifically, a design review of surface grading, retention with bleed off and offsite flow that impacts the site. The project will be designed and developed in accordance with the City of Scottsdale and Maricopa County's current development standards and client requirements.

1.2 Site Description

The proposed Deer Valley Townhomes development (Project) consists of attached townhomes split between three (3) buildings on a one acre parcel. The Site is defined by the parcel boundary for APN# 212-02-010E and is located at the northwest corner of Miller Road and Deer Valley Road in Scottsdale (see figure 1 below). The current project zoning is PCOC and proposed project zoning is R-3. The majority of the Site is undeveloped. A regional drainage channel exists along the east property boundary in approximately a 50' wide drainage channel. The proposed development will be constructed all at once and will not be phased.



Figure 1: Location Map

1.3 Watershed Description

The existing land use in the watershed is mainly single family residential with a commercial/office/retail generally at the major corners. The project is located in the northeast corner of the Lower Rawhide Wash watershed identified in the Pinnacle Peak West ADMS. For reference, there are figures from the ADMS in **Appendix D**. The Site has a smaller sub-watershed that contributes to the channel on site. In general, the watershed slopes from the northeast to the southwest and extends up to the neighborhoods along Hayden Road just north of Pinnacle Peak Road. There are two areas that are channelized and combine into one channel and pass under Miller Road. The channel continues south on the west side of Miller Road and flows into a box culvert at the northeast corner of our Site. Flows continue south, along on the east side of the parcel within a public drainage easement, and enter a box culvert under Deer Valley Road. The stormwater empties into the Grayhawk channel that flows from east to west on the south side of Deer Valley Road.

1.4 On-Site Topographic Conditions

The existing ground generally slopes from northeast to southwest at approximately 2%. Exhibits provided in **Appendix B** present the existing topographic conditions for the Project. Both Miller Road and Deer Valley Road are fully improved and catch basin with grate and curb inlet exists in the north curb line of Deer Valley.

1.5 FEMA Flood Insurance Map

The project is entirely located within Zone "X" according to Flood Insurance Rate Map (FIRM) Panel 04013C1320L which is effective October 16, 2013 (REF 1). Zone X is defined as: 0.2% Annual Chance Flood Hazard, Areas of 1% annual chance flood with average depth less than one foot or with drainage areas of less than one square mile. (Please refer to FIRMETTE in **Appendix A**).

2.0 Technical Analysis

2.1 FLO-2D

A FLO-2D analysis was performed for the Rawhide Wash Watershed as part of the Pinnacle Peak West ADMP (PPW ADMP). Flood Control District of Maricopa County provided access to the FLO-2D Web Access Tool at https://gis.maricopa.gov/FLO-2DModels. **Appendix D** contains map output from the model and it is based on 100-year, 24 hour storm event. Flows were used from the cells 507866 through 507868, equaling 429 cfs. Terrascape agrees and accepts these results for use in performing analysis for this Site. In discussions with staff from the City of Scottsdale Stormwater Management



division, the City stated that these flow rates could be used in our HEC-RAS analysis and it was suggested that we apply a factor of safety (FS). An FS of 1.3 was applied to the flow rate, resulting in Q_{100} =557 cfs. The flow rates in the FLO-2D model result in lower values than that listed in the 1996 data from Arizona Silverado Preliminary Drainage Plan (Q=739cfs). It is typical to see lower flow rates when using historical rainfall data in the FLO-2D model, versus the other floodplain modeling used in older studies.

2.2 HEC-RAS

The 100-year, 24 hour flow rate obtained from the PPW ADMP was used, with a 1.3 factor of safety, as input for the HEC-RAS model. The purpose of the model was to determine the water surface elevations (WSE) in the channel in order to set the lowest finished floor elevations for the residential structures. The WSE are shown on the Preliminary Grading and Drainage Plan found in **Appendix B**. Output from the model is found in **Appendix E**. Model results show that the regional flows are contained within the channel and within the Site and Deer Valley Road box culverts.

2.3 Stormwater Storage Facilities

The Site is being developed on a parcel that was excluded from the Arizona Silverado subdivision. Developer and the City originally envisioned this Site to be a commercial development. Evidence of this can be seen by previous submittals made to the City by other developers, and are cited in the reference section. The significance of this project history and how it relates to stormwater storage. This parcel was not conceptually planned with the intent to provide regional stormwater conveyance and on-site stormwater storage design. There is not enough surface area to provide stormwater detention basins and therefore stormwater detention facilities with a bleed-off pipe is not feasible. Upon development of this Project, any runoff that exceeds the capacity of the storage facility would occur and pass prior to regional peak. This is due to a Site time of concentration of 5 or 10 min, versus a regional watershed time of concentration of 13.4 hours (Refer to Channel Hydrograph in **Appendix C**).

The drainage channel along the eastern portion of the property consumes approximately 30% of the Parcel. This is a significant impediment to the property and supports the request for a Stormwater Storage Waiver which accompanies this report. The FLO-2D and the HEC-RAS analyses show that there is sufficient capacity in the channel to handle post-development flows from this Site. The application form for the waiver states the following condition:



"The development is adjacent to a conveyance facility that an engineering analysis shows is designed and constructed to handle the additional runoff from the site as a result of development."

Based on first flush design standard for computing retention volume, underground storage is proposed for this Project. The first flush volume calculation based on the Site's net area is based on Section 4-1.201 in the Design Standards & Policies Manual and provided in **Appendix C**.

2.4 Lowest Finished Floor Verification

All finished floors elevations have been set based on the water surface elevations in the adjacent channel. The Preliminary Grading & Drainage Plan is found in **Appendix B**. The northern 5-pack of townhouses is 2.93' above the WSE on the inlet side of the on-site culvert. The southern 2-pack along the channel is 1.93' higher than the SWE at the cross section on the outlet side of the on-site culvert.

The lowest elevation within the developed area is at a storm drain inlet within the trash turning maneuver area at the southwest corner. The elevation of the inlet is 75.50. If clogging or overflow occurs, the overtopping elevation is 76.00 for the top of curb adjacent to the inlet and on the east side of the driveway. Two locations are provided for ultimate outfalls; one at the southwest corner of the Site at elevation 75.0 and one into the channel at 74.60. Both locations route to the Greyhawk channel on the south side of Deer Valley Road.

2.5 Erosion Protection

It is our understanding that the regional channel was constructed with a minimum of 2' deep of 6" rip rap based on the 1996 Preliminary Drainage Plan for Arizona Silverado. Critical areas were specified as grouted rip rap, and evidence of this is seen at the inlet and outlet aprons to the box culverts on site. Terrascape made several attempts to obtain as-built plan data for Arizona Silverado subdivision from the City, engineering consultants, and the homeowner association. Data could not be located to determine the as-built channel plans. The aforementioned plan identified a design flow rate of 739 cfs. The rip rap should have been sized based on this flow, which is much larger than the flow rate in our analysis. Field observations indicate that the channel remains in good condition after 20 years and doesn't appear to have lateral migration.



Guideline 1 within State Standard Attachment 5-96, states that the section containing erosion setbacks applies to "Lateral Migration Setback Allowance for Riverine Floodplains in Arizona". The calculation for Level 1 analysis is:

Setback = $1.0(Q_{100})^{0.5}$

The minimum erosion setback is 20 feet for straight channels. Based on the calculation, the minimum setback calculation for the flow rate used in the analysis is 23.6 feet. A LOMR with an effective date of August 25, 2017 determined that the Site is located in Zone "X", along with the properties in the immediate vicinity. Since the on-site channel is lined with rip rap, and there is no defined floodway, an erosion setback is not required as the rip rap mitigates the concern for lateral migration.

3.0 Report Conclusions

The following conclusions have been reached as a result of this drainage investigation, in support of the proposed Deer Valley Townhomes Project:

- This drainage report was prepared in accordance with the recommendations and design parameters from the Design Standards & Policies Manual (REF 2), and MCFCD Drainage Design Manuals, Volume I and II (REF 4&5).
- The required retention volume is provided based on first flush based on 2.37-inches of run-off, per City of Scottsdale requirements and is designed to drain within 36 hours.
- Building lowest finished floor elevations for the Project exceed a minimum of 12inches above the 100-year 24-hour water surface elevations in the adjacent channel.



4.0 References

- Flood Insurance Rate Map, Maricopa County, Arizona, Map Number 04013C1320L, Federal Emergency Management Agency, Washington DC, October 16, 2013.
- 2. <u>Design Standards & Policies Manual</u>, City of Scottsdale, AZ, 2018.
- 3. <u>MAG Uniform Standard Details for Public Works Construction</u>, Maricopa Association of Governments, Phoenix, AZ, 2015 Revision.
- 4. <u>Drainage Design Manual for Maricopa County, Arizona Hydrology, 4th Edition,</u> Flood Control District of Maricopa County, Phoenix, AZ, August 15, 2013.
- 5. <u>Drainage Design Manual for Maricopa County, Arizona Hydraulics, 3rd Edition,</u> Flood Control District of Maricopa County, Phoenix, AZ, August 15, 2013.
- 6. <u>Watercourse System Sediment Balance</u>, State Standard Attachment 5-96, Arizona Department of Water Resources, September 1996.
- 7. <u>Preliminary Drainage Plan</u>, Hook Engineering, Inc., Phoenix, AZ, May 9, 1997.
- 8. Pinnacle Peak West Area Drainage Master Study: Draft Hydrology & Hydraulics Report, Volumes 1&2, Flood Control District of Maricopa County Project No. F0701, TYLIN International, July 26, 2013.
- Pinnacle Peak West Area Drainage Master Study: Rawhide Wash Alternatives Refinement, Flood Control District of Maricopa County, JE Fuller Hydrology & Geomorphology, Inc., June 2016.
- 10. Final Plat for Arizona Silverado, CMX Group, Inc., November 7, 1997.
- 11. <u>Preliminary Drainage Plan for Arizona Silverado</u>, Exhibit 1, Hook Engineering, Inc., May 9, 1997.
- 12. <u>Conceptual Grading & Drainage Plan for Convenience Store/Bank</u>, CMX Group, Inc., September 4, 1998.
- 13. <u>Grayhawk Deer Valley Channel, Phase 1</u>, Gilbertson Associates, Inc., March 31, 1995.
- 14. <u>Preliminary Drainage Report for Commercial Site Development</u>, Hook Engineering, Inc., October, 26, 2007.



Appendix A

Firmette

National Flood Hazard Layer FIRMette



eff. 10/16/201 LOMR 15-09-1857P LOMR 16-09-2931X eff. 6/10/2016 eff. 8/3/1/2016 LOMR 17-09-0074P eff. 8/25/2017 0.2 PCTANNUAL CHANGE FLOOD HAZARD CITY OF SCOTTSDALE DEPTH 1 Feet MEL4Feet/Second (DEPTH 1 Feet) MEL 4 Peet // Second MEL3 Feet / Second

DigitalGlobe, Geo Eye, Earthstar

1:6.000

Feet

2.000

250

500

1,000

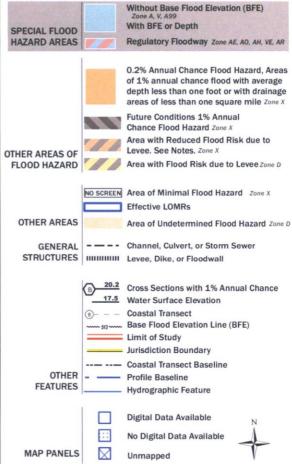
1,500

GS, AeroGRID, IGN, and the GIS User Community

33°40'49.44"N

Legend

SEE FIS REPORT FOR DETAILED LEGEND AND INDEX MAP FOR FIRM PANEL LAYOUT



This map complies with FEMA's standards for the use of digital flood maps if it is not void as described below. The base map shown complies with FEMA's base map accuracy standards

The flood hazard information is derived directly from the authoritative NFHL web services provided by FEMA. This map was exported on 4/26/2018 at 7:37:10 PM and does not reflect changes or amendments subsequent to this date and time. The NFHL and effective information may change or become superseded by new data over time.

This map image is void if the one or more of the following map elements do not appear: base map imagery, flood zone labels, legend, scale bar, map creation date, community identifiers, FIRM panel number, and FIRM effective date. Map images for unmapped and unmodernized areas cannot be used for regulatory purposes.

Appendix B

Drainage Exhibits & Existing Condition Maps

Existing Drainage Conditions

Deer Valley Townhomes

Deer Valley Road and Miller Road

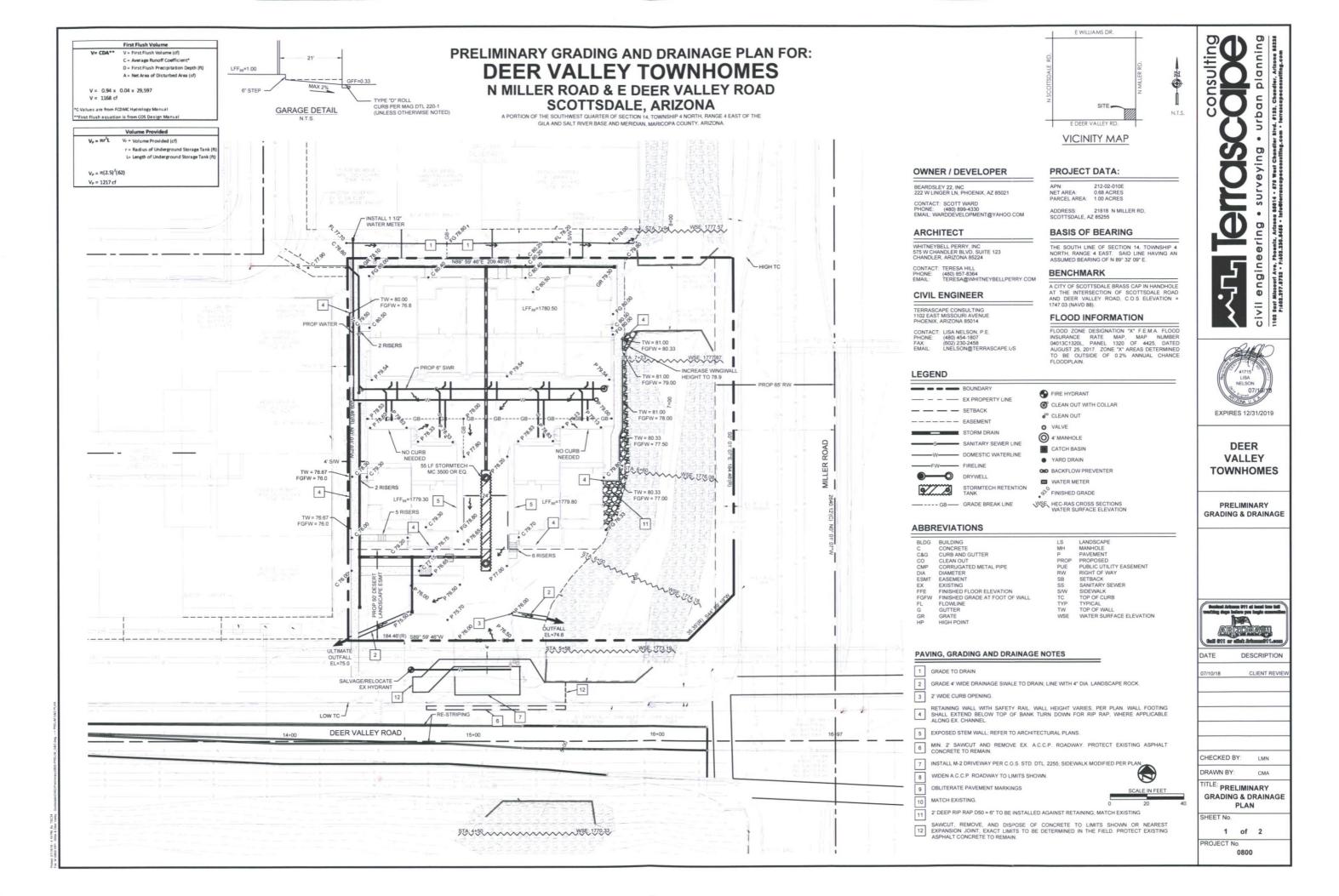
Project No. 0800

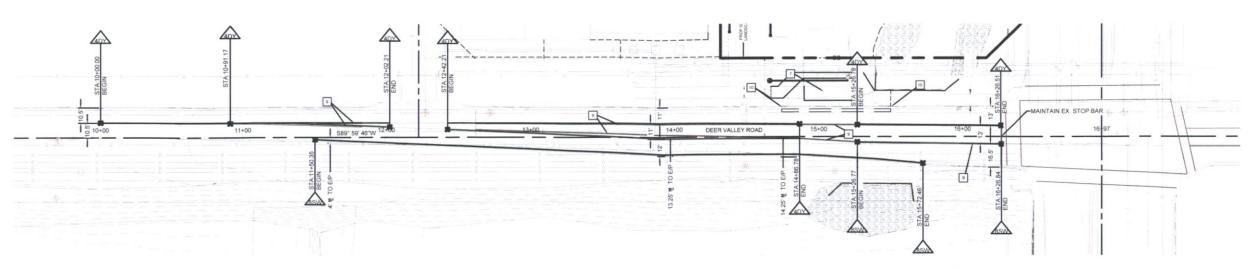
Date July 12, 2018

Terrascape consulting

civil engineering • surveying • urban planning

1102 East Missouri Ave, Phoenix, Arizona 85014 • 875 West Chandler Bivd. #123, Chandler, Arizona 85225 P:602.297.8732 • F:602.230.8458 • Info@terrascapeconsulting.com • terrascapeconsulting.com





PAVING, GRADING AND DRAINAGE NOTES 1 GRADE TO DRAIN 2 GRADE 4" WIDE DRAINAGE SWALE TO DRAIN; LINE WITH 4" DIA. LANDSCAPE ROCK. 3 2" WIDE CURB OPENING. 4 RETAINING WALL WITH SAFETY RAIL WALL HEIGHT VARIES, PER PLAN WALL FOOTING SHALL EXTEND BELOW TOP OF BANK TURN DOWN FOR RIP RAP, WHERE APPLICABLE ALONG EX. CHANNEL. 5 EXPOSED STEM WALL; REFER TO ARCHITECTURAL PLANS. 6 MIN. 2" SAWCUT AND REMOVE EX. A.C.C.P. ROADWAY. PROTECT EXISTING ASPHALT CONCRETE TO REMAIN. 7 DRIVEWAY PER C.O.S. STD. DTL. 2255, SIDEWALK MODIFIED PER PLAN. 8 WIDEN A.C.C.P. ROADWAY TO LIMITS SHOWN. 9 OBLITERATE PAVEMENT MARKINGS. 10 MATCH EXISTING. 11 2" DEEP RIP RAP D50 = 6" TO BE INSTALLED AGAINST RETAINING; MATCH EXISTING

civil engineering • surveying • urban planning



DEER VALLEY TOWNHOMES

PRELIMINARY GRADING & DRAINAGE



DATE DESCRIPTION

07/10/18 CLII

DRAWN BY:

TITLE: PRELIMINARY GRADING & DRAINAGE PLAN

SHEET No.

2 of 2

PROJECT No. 0800

SCALE IN FEET

0 30 60

Appendix C

Calculations

	经济市农场,则以为农场,通过大学的现在分词	First Flush Volume	
V= CDA**		V = First Flush Volume (cf)	
		C = Average Runoff Coefficient	•
		D = First Flush Precipitation De	pth (ft)
		A = Net Area of Disturbed Area	(sf)
V =	0.94 x	0.042 x	29,597
V =	1,168 cf		
*C-Values are from FCDMC Hydrology Manual			
**First Flush equation is from COS Design Manual			

		Volume Provided		
Number of chambers		6	Volume Per Chamber	110 cf
Number of End Caps		2	Volume Per End Cap	16 cf
Area		440 sf	Excavation Length	52 If
Perimeter		121 ft	Excavation Width	8 If
Stone above		12 in	Excavation Depth (Including cover)	6 If
Stone below		9 in		
Voids in stone		40 %		
Length of Isolator Row		47 ft		
Volume in chambers	# of Chambers * 109.9	659 cf		
Volume in End Caps	# of caps * 15.6	31 cf		
Volume of excavation	LXWXD	2422 cf		
Amount of stone	Vexc - Vchmb	1731 cf		
Volume in stone	Void % * Amount _{stone}	693 cf		
Amount of Filter Fabric	2*Area + Perimeter *(6 +Cover)	1822 sf		
Volume Provided	V _{chmb} + V _{stone}	1352 cf		

THE OWN DESCRIPTION OF THE PARTY OF THE PART	Pre vs. Post	The second secon
V = ΔC(R/12)A	V = Volume (cf)	
	ΔC = Change in Runoff Coefficient Over Disturbed Area*	
	R= Precipitation Amount (in)**	
	A= Disturbed Area (sf)	
$\Delta C = C_{post} - C_{pre}$		
= 0.94 - 0.44		
= 0.5		
$V = 0.50 \times (2.37/12) \times 29,597$		
V = 2,923 cf		
*C-Values are derived from FCDMC Hydrology Manual		
**100-year 2-hour precipitation from NOAA		



NOAA Atlas 14, Volume 1, Version 5 Location name: Scottsdale, Arizona, USA* Latitude: 33.6846°, Longitude: -111.9173° Elevation: 1777.81 ft**

* source: ESRI Maps ** source: USGS



POINT PRECIPITATION FREQUENCY ESTIMATES

Sanja Perica, Sarah Dietz, Sarah Heim, Lillian Hiner, Kazungu Maitaria, Deborah Martin, Sandra Pavlovic, Ishani Roy, Carl Trypaluk, Dale Unruh, Fenglin Yan, Michael Yekta, Tan Zhao, Geoffrey Bonnin, Daniel Brewer, Li-Chuan Chen, Tye Parzybok, John Yarchoan

NOAA, National Weather Service, Silver Spring, Maryland

PF tabular | PF graphical | Maps & aerials

PF tabular

PDS	S-based p	oint preci	pitation fr	equency e	estimates	with 90%	confidenc	e interval	s (in inch	nes) ¹
Duration				Averag	e recurrenc	e interval (y	ears)			
Duration	1	2	5	10	25	50	100	200	500	1000
5-min	0.203 (0.169-0.249)	0.265 (0.222-0.326)	0.358 (0.296-0.438)	0.429 (0.353-0.523)	0.524 (0.425-0.636)	0.597 (0.477-0.720)	0.671 (0.528-0.807)	0.745 (0.577-0.896)	0.845 (0.637-1.02)	0.921 (0.681-1.11)
10-min	0.309 (0.257-0.380)	0.404 (0.338-0.496)	0.545 (0.451-0.667)	0.653 (0.537-0.796)	0.798 (0.646-0.969)	0.908 (0.727-1.10)	1.02 (0.803-1.23)	1.13 (0.878-1.36)	1.29 (0.970-1.55)	1.40 (1.04-1.69)
15-min	0.384 (0.319-0.471)	0.500 (0.419-0.615)	0.676 (0.559-0.827)	0.810 (0.666-0.987)	0.989 (0.801-1.20)	1.13 (0.901-1.36)	1.27 (0.996-1.52)	1.41 (1.09-1.69)	1.59 (1.20-1.92)	1.74 (1.28-2.10)
30-min	0.516 (0.429-0.634)	0.674 (0.564-0.828)	0.910 (0.753-1.11)	1.09 (0.898-1.33)	1.33 (1.08-1.62)	1.52 (1.21-1.83)	1.71 (1.34-2.05)	1.89 (1.47-2.28)	2.15 (1.62-2.58)	2.34 (1.73-2.82)
60-min	0.639 (0.531-0.784)	0.834 (0.698-1.02)	1.13 (0.932-1.38)	1.35 (1.11-1.65)	1.65 (1.34-2.00)	1.88 (1.50-2.26)	2.11 (1.66-2.54)	2.34 (1.81-2.82)	2.66 (2.01-3.20)	2.90 (2.14-3.49)
2-hr	0.744 (0.626-0.894)	0.963 (0.813-1.16)	1.28 (1.07-1.54)	1.53 (1.26-1.83)	1.86 (1.52-2.21)	2.11 (1.71-2.50)	2.37 (1.88-2.81)	2.62 (2.06-3.11)	2.97 (2.28-3.52)	3.24 (2.43-3.86)
3-hr	0.814 (0.684-0.995)	1.04 (0.880-1.28)	1.36 (1.14-1.66)	1.62 (1.34-1.96)	1.97 (1.61-2.38)	2.25 (1.82-2.70)	2.54 (2.01-3.05)	2.85 (2.22-3.41)	3.26 (2.47-3.91)	3.60 (2.66-4.31)
6-hr	0.976 (0.840-1.16)	1.23 (1.06-1.46)	1.57 (1.35-1.86)	1.84 (1.56-2.17)	2.21 (1.85-2.59)	2.50 (2.06-2.91)	2.80 (2.27-3.26)	3.11 (2.48-3.62)	3.52 (2.73-4.10)	3.84 (2.92-4.48)
12-hr	1.12 (0.967-1.31)	1.41 (1.22-1.65)	1.77 (1.53-2.07)	2.06 (1.77-2.40)	2.46 (2.08-2.85)	2.75 (2.30-3.19)	3.07 (2.53-3.55)	3.38 (2.75-3.91)	3.79 (3.01-4.41)	4.11 (3.20-4.81)
24-hr	1.31 (1.15-1.52)	1.67 (1.46-1.93)	2.16 (1.89-2.50)	2.55 (2.22-2.95)	3.11 (2.68-3.58)	3.55 (3.03-4.08)	4.01 (3.39-4.62)	4.49 (3.75-5.18)	5.16 (4.23-5.98)	5.70 (4.60-6.65)
2-day	1.44 (1.25-1.66)	1.84 (1.60-2.12)	2.41 (2.10-2.77)	2.87 (2.49-3.30)	3.52 (3.02-4.04)	4.03 (3.43-4.63)	4.58 (3.86-5.27)	5.15 (4.29-5.95)	5.95 (4.87-6.91)	6.59 (5.32-7.71)
3-day	1.54 (1.35-1.77)	1.98 (1.73-2.26)	2.61 (2.28-2.98)	3.12 (2.72-3.56)	3.85 (3.33-4.39)	4.44 (3.80-5.07)	5.07 (4.30-5.81)	5.73 (4.81-6.60)	6.68 (5.50-7.73)	7.45 (6.05-8.69)
4-day	1.65 (1.45-1.88)	2.11 (1.86-2.41)	2.81 (2.47-3.19)	3.37 (2.95-3.82)	4.18 (3.63-4.75)	4.84 (4.17-5.51)	5.56 (4.74-6.34)	6.32 (5.33-7.25)	7.41 (6.14-8.56)	8.31 (6.78-9.67)
7-day	1.87 (1.64-2.15)	2.40 (2.10-2.74)	3.19 (2.79-3.65)	3.84 (3.34-4.38)	4.77 (4.12-5.44)	5.53 (4.74-6.32)	6.35 (5.39-7.29)	7.24 (6.06-8.35)	8.50 (7.00-9.88)	9.55 (7.74-11.2)
10-day	2.04 (1.79-2.33)	2.61 (2.30-2.99)	3.47 (3.04-3.95)	4.17 (3.63-4.74)	5.16 (4.47-5.87)	5.97 (5.12-6.80)	6.84 (5.81-7.81)	7.77 (6.53-8.92)	9.09 (7.51-10.5)	10.2 (8.27-11.9)
20-day	2.54 (2.24-2.90)	3.28 (2.89-3.73)	4.34 (3.81-4.92)	5.16 (4.51-5.84)	6.27 (5.46-7.12)	7.15 (6.18-8.12)	8.05 (6.92-9.19)	8.99 (7.65-10.3)	10.3 (8.63-11.9)	11.3 (9.37-13.1)
30-day	3.00 (2.63-3.41)	3.86 (3.40-4.39)	5.10 (4.48-5.79)	6.06 (5.31-6.86)	7.36 (6.41-8.34)	8.37 (7.24-9.49)	9.42 (8.10-10.7)	10.5 (8.94-11.9)	12.0 (10.1-13.7)	13.1 (10.9-15.1)
45-day	3.52 (3.11-3.99)	4.54 (4.01-5.15)	6.00 (5.30-6.79)	7.11 (6.25-8.04)	8.59 (7.51-9.73)	9.73 (8.45-11.0)	10.9 (9.40-12.4)	12.1 (10.3-13.8)	13.7 (11.6-15.8)	14.9 (12.5-17.4)
60-day	3.92 (3.47-4.43)	5.07 (4.49-5.73)	6.69 (5.91-7.54)	7.88 (6.94-8.89)	9.46 (8.29-10.7)	10.7 (9.28-12.1)	11.9 (10.3-13.5)	13.1 (11.2-14.9)	14.7 (12.5-16.9)	15.9 (13.4-18.5)

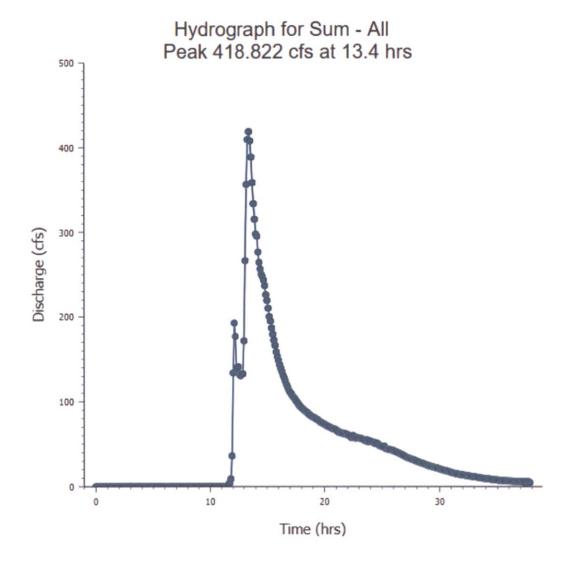
¹ Precipitation frequency (PF) estimates in this table are based on frequency analysis of partial duration series (PDS).

Numbers in parenthesis are PF estimates at lower and upper bounds of the 90% confidence interval. The probability that precipitation frequency estimates (for a given duration and average recurrence interval) will be greater than the upper bound (or less than the lower bound) is 5%. Estimates at upper bounds are not checked against probable maximum precipitation (PMP) estimates and may be higher than currently valid PMP values.

Please refer to NOAA Atlas 14 document for more information.

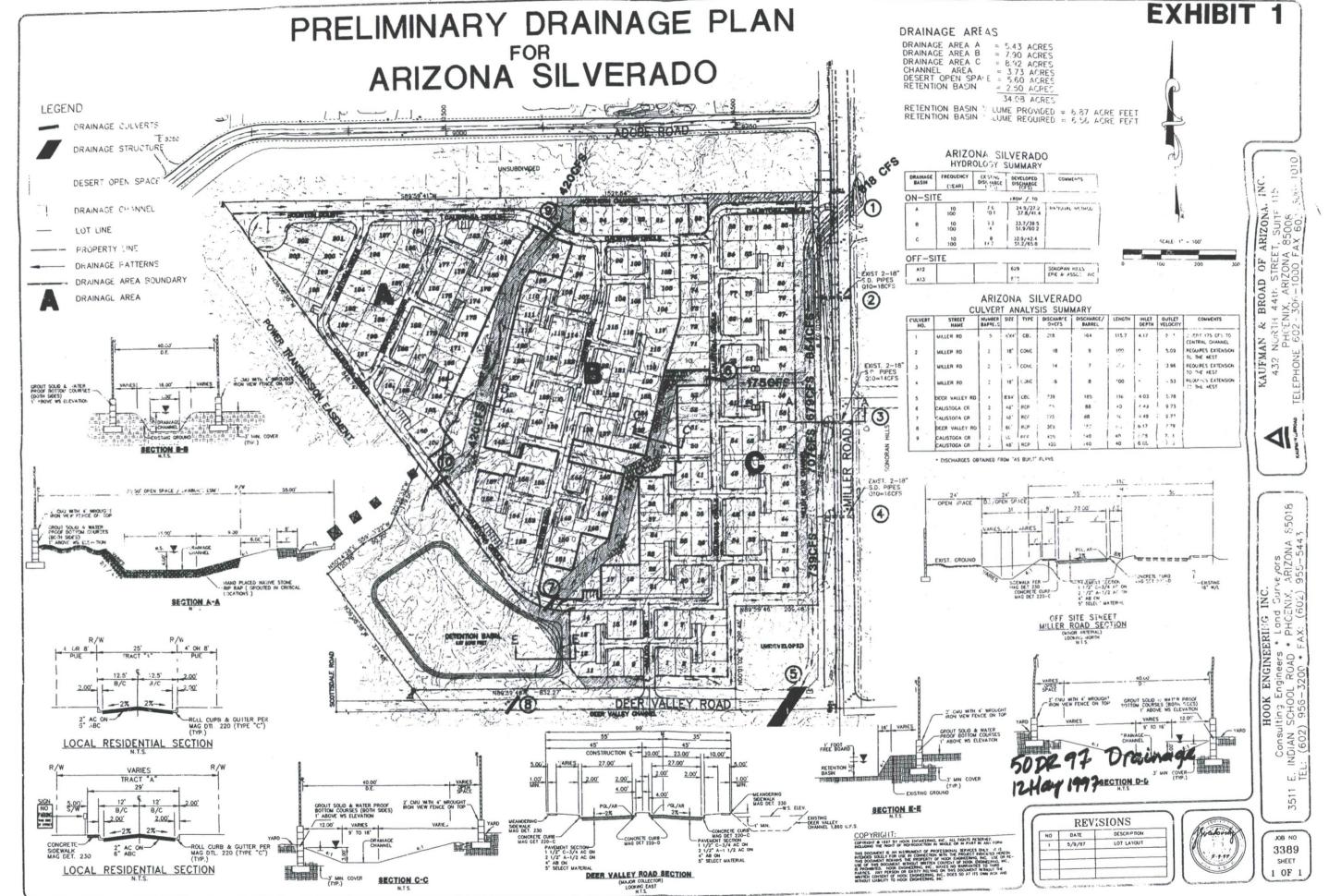
Back to Top

PF graphical



Appendix D

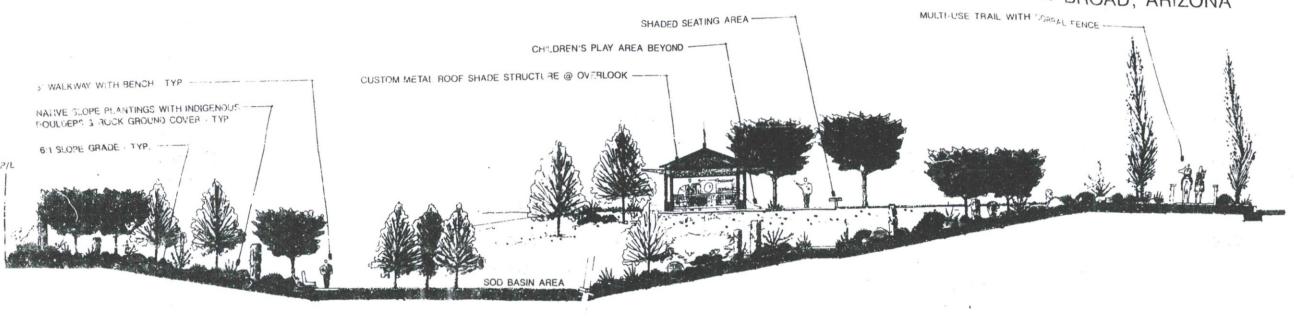
Supplemental Information



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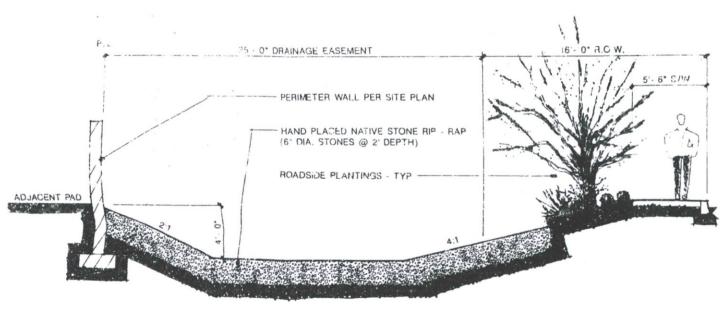
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ARIZONA SILVERADO KAUFMAN AND BROAD, ARIZONA



SECTION A - A

SECTION B - B



-1" THICK RUSTED STEEL PLATE WITH SCALLOPED EDGE - LARGE TERRA COTTA FLOWER POTS ON INDIGENOUS STONE PEDESTAL - TO - POURED IN PLACE CONCRETE SIGN WALL WITH BRASS PIN-TYPE LETTERS (BACK-UT OVER A SANDBLASTED DESIGN FINISH - LOW INDIGENOUS STATE PLANTER

ENTRY SIGNAGE ELEVATION

CONCEPTUAL SITE SECTIONS AND ELEVATIONS

JANUARY 17, 1997

Pinnacle Peak West ADMS Executive Summary

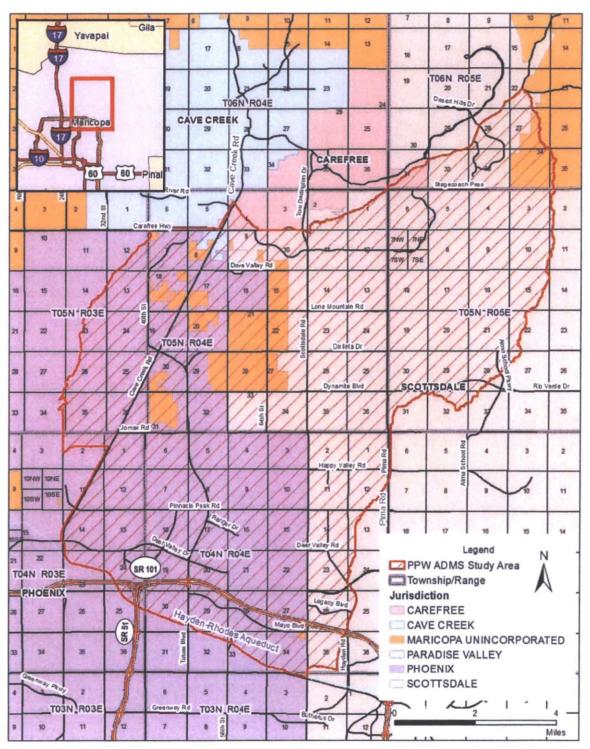


Figure 1. PPW ADMS Vicinity Map

Pinnacle Peak West ADMS Executive Summary

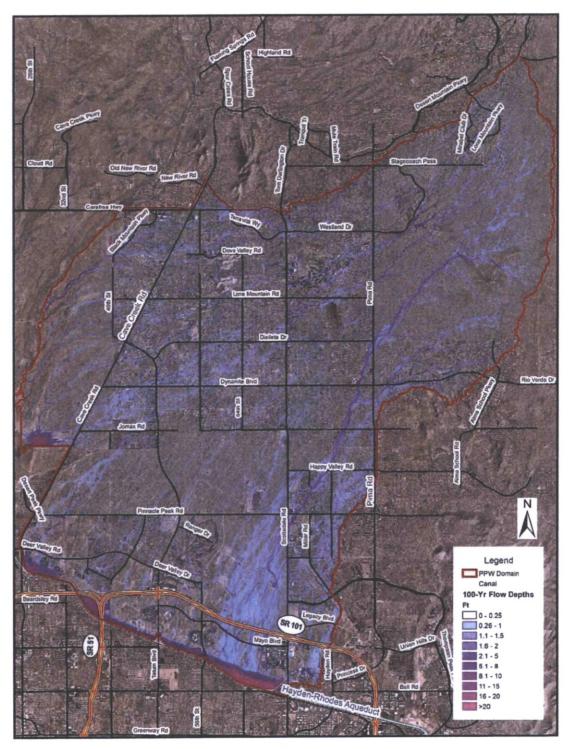
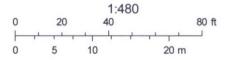


Figure 3. 100-Year Flow Depth Results

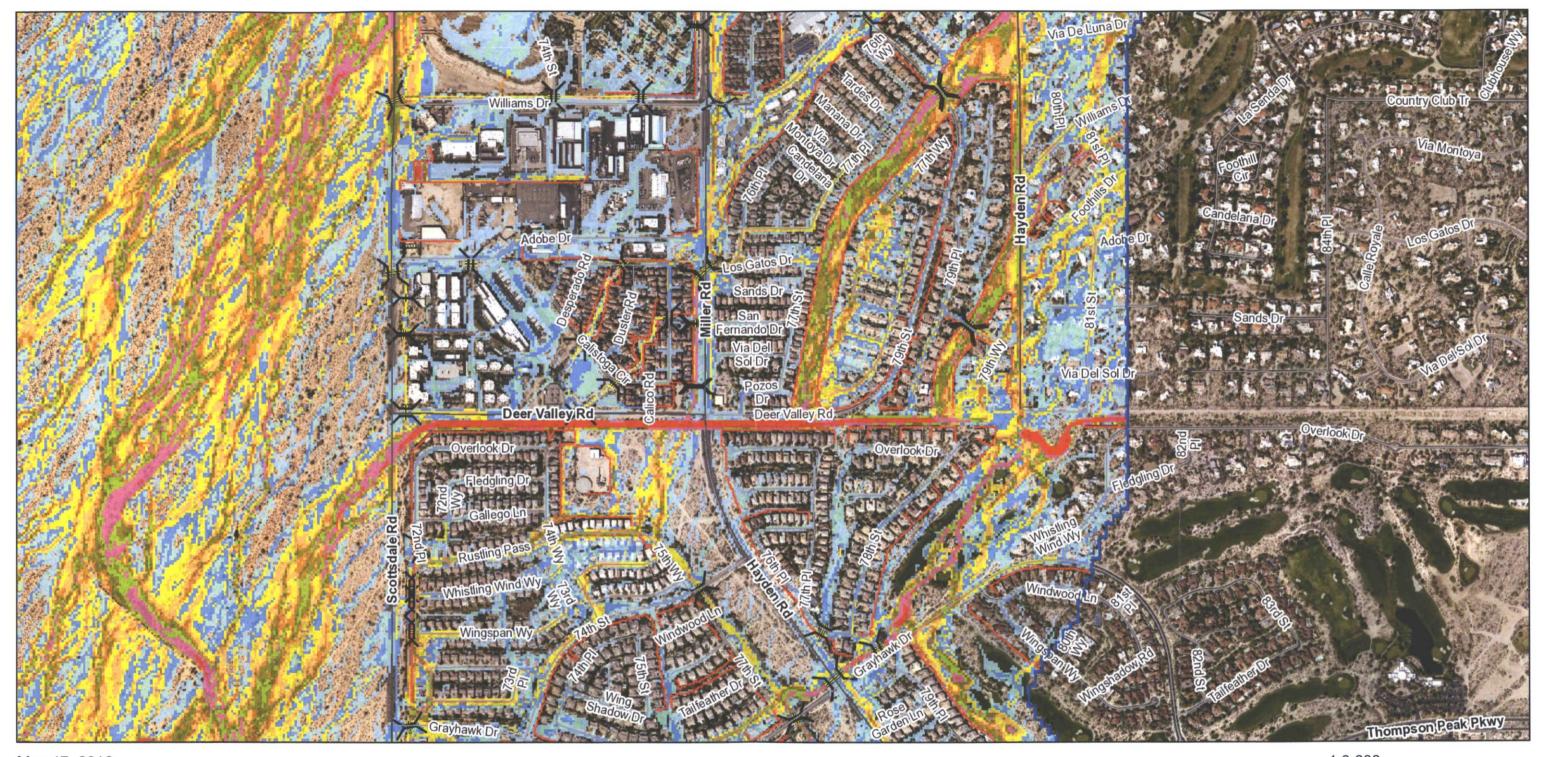
121_PinnaclePeakWest - Lower Rawhide 100YR24HR With Walls

		10		1 6		505673			
	506399 506400	506401 50640	2 506403	506404	506405	1782.3 ft 40.71 cfs 506406	506407	506408	STATE OF THE PARTY
	1779.32 ft 1779.33 ft 55.23 cfs 343 cfs	1781.05 ft 1781.38 1.66 cfs 7.19 c	PERSONAL PROPERTY AND	1782.02 ft 6.36 cfs	1782.02 ft 16.45 cfs	1781.92 ft 40.75 cfs	1782.13 ft 6.56 cfs	1782.5 ft 1.59 cfs	
	507132 507133	507134 50713	5 507136	507137	507138	507139	507140		et all the
	1778.56 ft 1778.34 ft 65.79 cfs 342.62 cfs	1780.36 ft 3.36 cfs 10.61 d		781.66 ft 4.34 cfs	1781.65 ft 15.56 cfs	1781.57 ft 38.98 cfs	1781.67 ft 8.12 cfs		· · · · · · · · · · · · · · · · · · ·
	507866 507867	507868 50786	9 507870	507871	507872	507873	507874	S. All	
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THE ALL MAN	4.35 cfs 58.78 cfs	1779:16 ft 1780.01 10:96 cfs 5.73 c		2.75 cfs	1780.93 ft 15.69 cfs	38.03 cfs	5.85 cfs	- Prof	の事業を
-		509336 50933 1779.1 ft 1779.57		509339 1780.62 ft	509340 1780.53 ft	509341 1780.43 ft	509342 1780.5 ft	509343 1780.73 ft	
1		3.98 cfs 3.89 c		2.37 cfs	12.5 cfs	35.77 cfs	10.86 cfs	2.77 cfs	
11 9 11 11 11	510069 510070 1777.21 ft 1777.3 ft	510071 51007 1779.05 ft 1779.23	8 ft 1779.76 ft	510074 1780.25 ft	510075 1780.21 ft	510076 1780.17 ft	510077 1780.31 ft		510079 1780.79 ft
510803	197.25 cfs 262.49 cfs 510804 510805	1.94 cfs 2.72 c		2.06 cfs 510809	12.47 cfs 510810	37.51 cfs 510811	10.03 cfs 510812	al e	1.27 cfs
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511538	511539 511540	511541 51154		511544	511545	511546			
1776.67 m 14.11 cfs	1776.68 ft 1776.72 ft 251.64 cfs 166.64 cfs	1778.84 ft 1779.13 2.05 cfs 3.16 c		1779.8 ft 2.49 cfs	1779.85 ft 19.8 cfs	1779.85 ft 33.26 cfs	F. Sec.	1	1000
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1775.69 ft 1.23 cfs 1776.37 ft 4.88 cfs 19.46 cfs	1776.47 ft 1776.48 ft 267.77 cfs 148.61 cfs	1778.72 ft 1779.06 2.27 cfs 3.65 c		779.64 ft 4.25 cfs	1779.71 ft 20.87 cfs	1779.72 ft 30.3 cfs			
513009 513010	513011 513012	513013 51301		513016	513017	513018			
1776.01 ft 1776.13 ft 13.65 cfs 21.65 cfs	1776.21 ft 1776.22 ft 282.57 cfs 120.85 cfs	1778.61 ft 1778.94 2.62 cfs 5.14 c	ALL SOLD STATE OF THE PARTY AND ADDRESS OF THE	1779.48 ft 5.54 cfs	1779.59 ft 19.2 cfs	1779.61 ft 27.08 cfs			
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5.35 cfs 9.58 cfs 9.42 cfs	327.91 cfs 95.58 cfs	6.39 cfs 6.17 c	fs 4.96 cfs	5.27 cfs	17.23 cfs	23.7 cfs	35		
514482 514483 514485 1775.16 ft 1775.18 ft 1774.9 ft	514486 514487 1774.63 ft 1775.7 ft	514488 51448 1778.56 ft 1778.78		514491 1779.24 ft	514492 1779.3 ft	514493 1779.31 ft			
2.96 cfs 9.19 cfs 59.02 cfs	358.94 cfs 11.19 cfs	4.62 cfs 4.63 c		4.47 cfs	15.31 cfs	21.51 cfs	E 100		

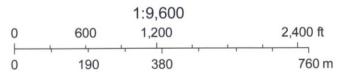
July 13, 2018



121_PinnaclePeakWest - Lower Rawhide 100YR24HR With Walls



May 17, 2018 0 600







Deer Valley Townhomes at Miller Rd and Deer Valley Rd

Scottsdale, Arizona

STORMTECH CHAMBER SPECIFICATIONS

- CHAMBERS SHALL BE STORMTECH MC-3500 OR APPROVED EQUAL.
- 2. CHAMBERS SHALL BE MADE FROM VIRGIN, IMPACT-MODIFIED POLYPROPYLENE COPOLYMERS
- CHAMBER ROWS SHALL PROVIDE CONTINUOUS, UNOBSTRUCTED INTERNAL SPACE WITH NO INTERNAL SUPPORT PANELS THAT WOULD IMPEDE FLOW OR LIMIT ACCESS FOR INSPECTION.
- 4. THE STRUCTURAL DESIGN OF THE CHAMBERS, THE STRUCTURAL BACKFILL, AND THE INSTALLATION REQUIREMENTS SHALL ENSURE THAT THE LOAD FACTORS SPECIFIED IN THE AASHTO LRFD BRIDGE DESIGN SPECIFICATIONS, SECTION 12.12, ARE MET FOR: 1) LONG-DURATION DEAD LOADS AND 2) SHORT-DURATION LIVE LOADS, BASED ON THE AASHTO DESIGN TRUCK WITH CONSIDERATION FOR IMPACT AND MULTIPLE VEHICLE PRESENCES.
- CHAMBERS SHALL MEET THE REQUIREMENTS OF ASTM F2418, "STANDARD SPECIFICATION FOR POLYPROPYLENE (PP) CORRUGATED WALL STORMWATER COLLECTION CHAMBERS".
- CHAMBERS SHALL BE DESIGNED AND ALLOWABLE LOADS DETERMINED IN ACCORDANCE WITH ASTM F2787, "STANDARD PRACTICE FOR STRUCTURAL DESIGN OF THERMOPLASTIC CORRUGATED WALL STORMWATER COLLECTION CHAMBERS".
- ONLY CHAMBERS THAT ARE APPROVED BY THE SITE DESIGN ENGINEER WILL BE ALLOWED. THE CHAMBER MANUFACTURER SHALL SUBMIT THE FOLLOWING UPON REQUEST TO THE SITE DESIGN ENGINEER FOR APPROVAL BEFORE DELIVERING CHAMBERS TO THE PROJECT SITE:
 - a. A STRUCTURAL EVALUATION SEALED BY A REGISTERED PROFESSIONAL ENGINEER THAT DEMONSTRATES THAT THE SAFETY FACTORS ARE GREATER THAN OR EQUAL TO 1.95 FOR DEAD LOAD AND 1.75 FOR LIVE LOAD, THE MINIMUM REQUIRED BY ASTM F2787 AND BY AASHTO FOR THERMOPLASTIC PIPE.
 - b. A STRUCTURAL EVALUATION SEALED BY A REGISTERED PROFESSIONAL ENGINEER THAT DEMONSTRATES THAT THE LOAD FACTORS SPECIFIED IN THE AASHTO LRFD BRIDGE DESIGN SPECIFICATIONS, SECTION 12.12, ARE MET. THE 50 YEAR CREEP MODULUS DATA SPECIFIED IN ASTM F2418 MUST BE USED AS PART OF THE AASHTO STRUCTURAL EVALUATION TO VERIFY LONG-TERM PERFORMANCE.
 - c. STRUCTURAL CROSS SECTION DETAIL ON WHICH THE STRUCTURAL EVALUATION IS BASED.
- 8. CHAMBERS AND END CAPS SHALL BE PRODUCED AT AN ISO 9001 CERTIFIED MANUFACTURING FACILITY.

IMPORTANT - NOTES FOR THE BIDDING AND INSTALLATION OF MC-3500 CHAMBER SYSTEM

- STORMTECH MC-3500 CHAMBERS SHALL NOT BE INSTALLED UNTIL THE MANUFACTURER'S REPRESENTATIVE HAS COMPLETED A
 PRE-CONSTRUCTION MEETING WITH THE INSTALLERS.
- 2. STORMTECH MC-3500 CHAMBERS SHALL BE INSTALLED IN ACCORDANCE WITH THE "STORMTECH MC-3500/MC-4500 CONSTRUCTION GUIDE".
- 3. CHAMBERS ARE NOT TO BE BACKFILLED WITH A DOZER OR AN EXCAVATOR SITUATED OVER THE CHAMBERS.

STORMTECH RECOMMENDS 3 BACKFILL METHODS:

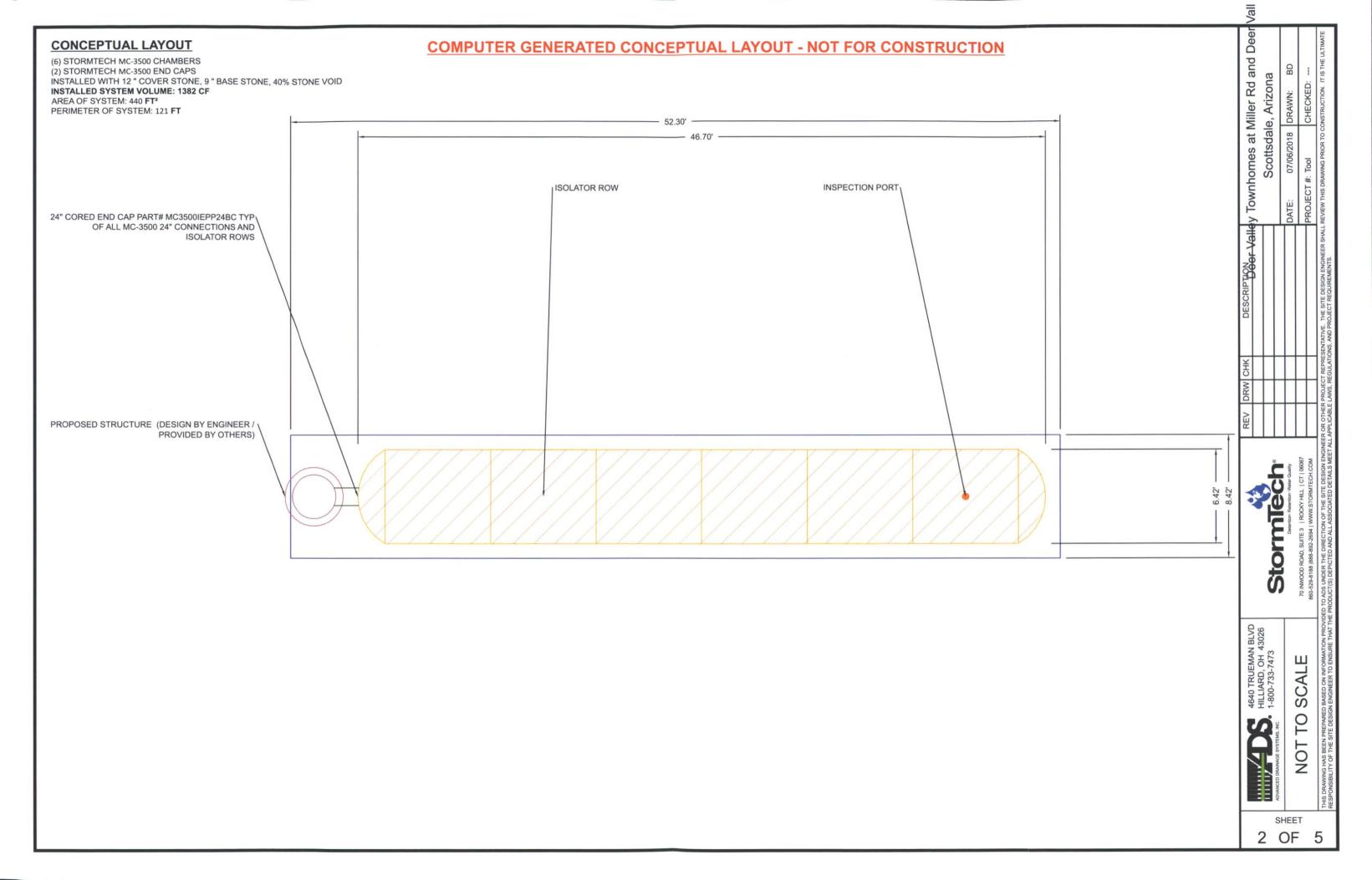
- STONESHOOTER LOCATED OFF THE CHAMBER BED.
- BACKFILL AS ROWS ARE BUILT USING AN EXCAVATOR ON THE FOUNDATION STONE OR SUBGRADE.
- BACKFILL FROM OUTSIDE THE EXCAVATION USING A LONG BOOM HOE OR EXCAVATOR.
- 4. THE FOUNDATION STONE SHALL BE LEVELED AND COMPACTED PRIOR TO PLACING CHAMBERS.
- 5. JOINTS BETWEEN CHAMBERS SHALL BE PROPERLY SEATED PRIOR TO PLACING STONE.
- 6. MAINTAIN MINIMUM 9" (230 mm) SPACING BETWEEN THE CHAMBER ROWS.
- 7. INLET AND OUTLET MANIFOLDS MUST BE INSERTED A MINIMUM OF 12" (300 mm) INTO CHAMBER END CAPS.
- EMBEDMENT STONE SURROUNDING CHAMBERS MUST BE A CLEAN, CRUSHED, ANGULAR STONE 3/4-2" (20-50 mm) MEETING THE AASHTO M43
 DESIGNATION OF #3 OR #4.
- 9. STONE MUST BE PLACED ON THE TOP CENTER OF THE CHAMBER TO ANCHOR THE CHAMBERS IN PLACE AND PRESERVE ROW SPACING..
- 10. ADS RECOMMENDS THE USE OF "FLEXSTORM CATCH IT" INSERTS DURING CONSTRUCTION FOR ALL INLETS TO PROTECT THE SUBSURFACE STORMWATER MANAGEMENT SYSTEM FROM CONSTRUCTION SITE RUNOFF.

NOTES FOR CONSTRUCTION EQUIPMENT

- STORMTECH MC-3500 CHAMBERS SHALL BE INSTALLED IN ACCORDANCE WITH THE "STORMTECH MC-3500/MC-4500 CONSTRUCTION GUIDE".
- THE USE OF EQUIPMENT OVER MC-3500 CHAMBERS IS LIMITED:
 - NO EQUIPMENT IS ALLOWED ON BARE CHAMBERS.
 - NO RUBBER TIRED LOADER, DUMP TRUCK, OR EXCAVATORS ARE ALLOWED UNTIL PROPER FILL DEPTHS ARE REACHED IN ACCORDANCE WITH THE "STORMTECH MC-3500/MC-4500 CONSTRUCTION GUIDE".
 - WEIGHT LIMITS FOR CONSRUCTION EQUIPMENT CAN BE FOUND IN THE "STORMTECH MC-3500/MC-4500 CONSTRUCTION GUIDE"
- 3. FULL 36" (900 mm) OF STABILIZED COVER MATERIALS OVER THE CHAMBERS IS REQUIRED FOR DUMP TRUCK TRAVEL OR DUMPING.

USE OF A DOZER TO PUSH EMBEDMENT STONE BETWEEN THE ROWS OF CHAMBERS MAY CAUSE DAMAGE TO CHAMBERS AND IS NOT AN ACCEPTABLE BACKFILL METHOD. ANY CHAMBERS DAMAGED BY USING THE "DUMP AND PUSH" METHOD ARE NOT COVERED UNDER THE STORMTECH STANDARD WARRANTY

CONTACT STORMTECH AT 1-888-892-2694 WITH ANY QUESTIONS ON INSTALLATION REQUIREMENTS OR WEIGHT LIMITS FOR CONSTRUCTION EQUIPMENT.

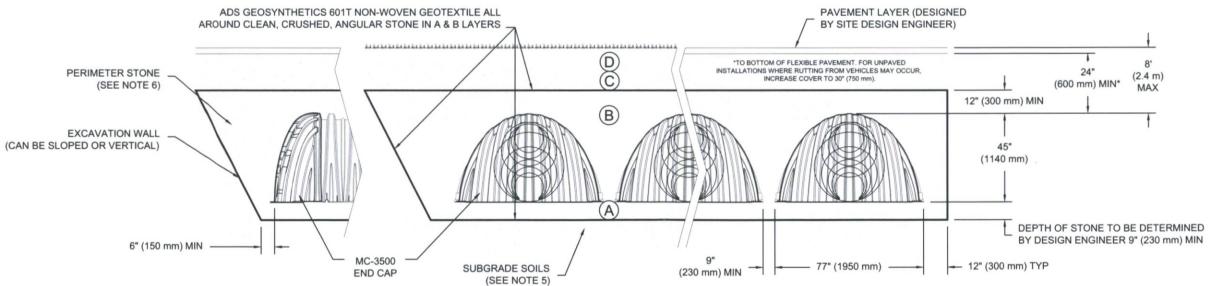


ACCEPTABLE FILL MATERIALS: STORMTECH MC-3500 CHAMBER SYSTEMS

	MATERIAL LOCATION	DESCRIPTION	AASHTO MATERIAL CLASSIFICATIONS	COMPACTION / DENSITY REQUIREMENT
D	FINAL FILL: FILL MATERIAL FOR LAYER 'D' STARTS FROM THE TOP OF THE 'C' LAYER TO THE BOTTOM OF FLEXIBLE PAVEMENT OR UNPAVED FINISHED GRADE ABOVE. NOTE THAT PAVEMENT SUBBASE MAY BE PART OF THE 'D' LAYER	ANY SOIL/ROCK MATERIALS, NATIVE SOILS, OR PER ENGINEER'S PLANS. CHECK PLANS FOR PAVEMENT SUBGRADE REQUIREMENTS.	N/A	PREPARE PER SITE DESIGN ENGINEER'S PLANS. PAVED INSTALLATIONS MAY HAVE STRINGENT MATERIAL AND PREPARATION REQUIREMENTS.
С	INITIAL FILL: FILL MATERIAL FOR LAYER 'C' STARTS FROM THE TOP OF THE EMBEDMENT STONE ('B' LAYER) TO 24" (600 mm) ABOVE THE TOP OF THE CHAMBER. NOTE THAT PAVEMENT SUBBASE MAY BE A PART OF THE 'C' LAYER.	GRANULAR WELL-GRADED SOIL/AGGREGATE MIXTURES, <35% FINES OR PROCESSED AGGREGATE. MOST PAVEMENT SUBBASE MATERIALS CAN BE USED IN LIEU OF THIS LAYER.	AASHTO M145 ¹ A-1, A-2-4, A-3 OR AASHTO M43 ¹ 3, 357, 4, 467, 5, 56, 57, 6, 67, 68, 7, 78, 8, 89, 9, 10	BEGIN COMPACTIONS AFTER 24" (600 mm) OF MATERIAL OVER THE CHAMBERS IS REACHED. COMPACT ADDITIONAL LAYERS IN 12" (300 mm) MAX LIFTS TO A MIN. 95% PROCTOR DENSITY FOR WELL GRADED MATERIAL AND 95% RELATIVE DENSITY FOR PROCESSED AGGREGATE MATERIALS.
В	EMBEDMENT STONE: FILL SURROUNDING THE CHAMBERS FROM THE FOUNDATION STONE ('A' LAYER) TO THE 'C' LAYER ABOVE.	CLEAN, CRUSHED, ANGULAR STONE, NOMINAL SIZE DISTRIBUTION BETWEEN 3/4-2 INCH (20-50 mm)	AASHTO M43 ¹ 3, 4	NO COMPACTION REQUIRED.
А	FOUNDATION STONE: FILL BELOW CHAMBERS FROM THE SUBGRADE UP TO THE FOOT (BOTTOM) OF THE CHAMBER.	CLEAN, CRUSHED, ANGULAR STONE, NOMINAL SIZE DISTRIBUTION BETWEEN 3/4-2 INCH (20-50 mm)	AASHTO M43 ¹ 3, 4	PLATE COMPACT OR ROLL TO ACHIEVE A FLAT SURFACE. 2 3

PLEASE NOTE:

- 1. THE LISTED AASHTO DESIGNATIONS ARE FOR GRADATIONS ONLY. THE STONE MUST ALSO BE CLEAN, CRUSHED, ANGULAR. FOR EXAMPLE, A SPECIFICATION FOR #4 STONE WOULD STATE: "CLEAN, CRUSHED, ANGULAR NO. 4 (AASHTO M43) STONE".
- 2. STORMTECH COMPACTION REQUIREMENTS ARE MET FOR 'A' LOCATION MATERIALS WHEN PLACED AND COMPACTED IN 9" (230 mm) (MAX) LIFTS USING TWO FULL COVERAGES WITH A VIBRATORY COMPACTOR.
- 3. WHERE INFILTRATION SURFACES MAY BE COMPROMISED BY COMPACTION, FOR STANDARD DESIGN LOAD CONDITIONS, A FLAT SURFACE MAY BE ACHIEVED BY RAKING OR DRAGGING WITHOUT COMPACTION EQUIPMENT. FOR SPECIAL LOAD DESIGNS, CONTACT STORMTECH FOR COMPACTION REQUIREMENTS.



NOTES:

- 1. MC-3500 CHAMBERS SHALL CONFORM TO THE REQUIREMENTS OF ASTM F2418 "STANDARD SPECIFICATION FOR POLYPROPYLENE (PP) CORRUGATED WALL STORMWATER COLLECTION CHAMBERS".
- 2. MC-3500 CHAMBERS SHALL BE DESIGNED IN ACCORDANCE WITH ASTM F2787 "STANDARD PRACTICE FOR STRUCTURAL DESIGN OF THERMOPLASTIC CORRUGATED WALL STORMWATER COLLECTION CHAMBERS".
- 3. "ACCEPTABLE FILL MATERIALS" TABLE ABOVE PROVIDES MATERIAL LOCATIONS, DESCRIPTIONS, GRADATIONS, AND COMPACTION REQUIREMENTS FOR FOUNDATION, EMBEDMENT, AND FILL MATERIALS.
- 4. THE "SITE DESIGN ENGINEER" REFERS TO THE ENGINEER RESPONSIBLE FOR THE DESIGN AND LAYOUT OF THE STORMTECH CHAMBERS FOR THIS PROJECT.
- 5. THE SITE DESIGN ENGINEER IS RESPONSIBLE FOR ASSESSING THE BEARING RESISTANCE (ALLOWABLE BEARING CAPACITY) OF THE SUBGRADE SOILS AND THE DEPTH OF FOUNDATION STONE WITH CONSIDERATION FOR THE RANGE OF EXPECTED SOIL MOISTURE CONDITIONS.
- 6. PERIMETER STONE MUST BE EXTENDED HORIZONTALLY TO THE EXCAVATION WALL FOR BOTH VERTICAL AND SLOPED EXCAVATION WALLS.
- 7. ONCE LAYER 'C' IS PLACED, ANY SOIL/MATERIAL CAN BE PLACED IN LAYER 'D' UP TO THE FINISHED GRADE. MOST PAVEMENT SUBBASE SOILS CAN BE USED TO REPLACE THE MATERIAL REQUIREMENTS OF LAYER 'C' OR 'D' AT THE SITE DESIGN ENGINEER'S DISCRETION.

Dee and BD Townhomes at Miller Rd Scottsdale, Arizona StormTe

3 OF

INSPECTION & MAINTENANCE

STEP 1) INSPECT ISOLATOR ROW FOR SEDIMENT

A. INSPECTION PORTS (IF PRESENT)

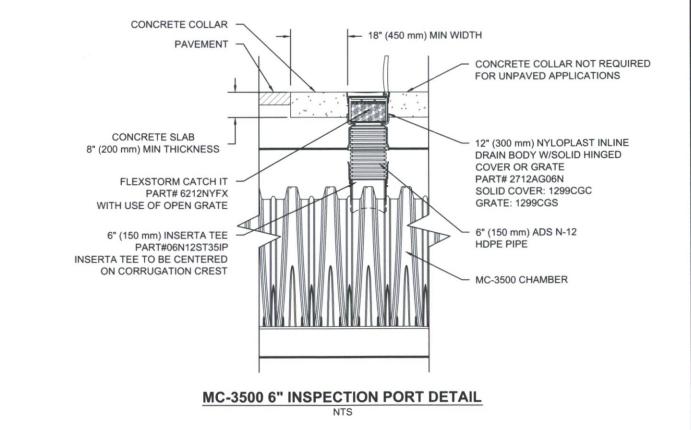
- A.1. REMOVE/OPEN LID ON NYLOPLAST INLINE DRAIN
- A.2. REMOVE AND CLEAN FLEXSTORM FILTER IF INSTALLED
- A.3. USING A FLASHLIGHT AND STADIA ROD, MEASURE DEPTH OF SEDIMENT AND RECORD ON MAINTENANCE LOG
- A.4. LOWER A CAMERA INTO ISOLATOR ROW FOR VISUAL INSPECTION OF SEDIMENT LEVELS (OPTIONAL)
- A.5. IF SEDIMENT IS AT, OR ABOVE, 3" (80 mm) PROCEED TO STEP 2. IF NOT, PROCEED TO STEP 3.

B. ALL ISOLATOR ROWS

- B.1. REMOVE COVER FROM STRUCTURE AT UPSTREAM END OF ISOLATOR ROW
- B.2. USING A FLASHLIGHT, INSPECT DOWN THE ISOLATOR ROW THROUGH OUTLET PIPE
 - i) MIRRORS ON POLES OR CAMERAS MAY BE USED TO AVOID A CONFINED SPACE ENTRY
 - ii) FOLLOW OSHA REGULATIONS FOR CONFINED SPACE ENTRY IF ENTERING MANHOLE IF SEDIMENT IS AT, OR ABOVE, 3" (80 mm) PROCEED TO STEP 2. IF NOT, PROCEED TO STEP 3.
- B.3. IF SEDIMENT IS AT, OR ABOVE, 3 (80 IIIII) PROCEED TO STEP 2. IF NOT, PROCEED TO STE
- STEP 2) CLEAN OUT ISOLATOR ROW USING THE JETVAC PROCESS
 - A. A FIXED CULVERT CLEANING NOZZLE WITH REAR FACING SPREAD OF 45" (1.1 m) OR MORE IS PREFERRED
 - B. APPLY MULTIPLE PASSES OF JETVAC UNTIL BACKFLUSH WATER IS CLEAN
 - C. VACUUM STRUCTURE SUMP AS REQUIRED
- STEP 3) REPLACE ALL COVERS, GRATES, FILTERS, AND LIDS; RECORD OBSERVATIONS AND ACTIONS.
- STEP 4) INSPECT AND CLEAN BASINS AND MANHOLES UPSTREAM OF THE STORMTECH SYSTEM.

NOTES

- INSPECT EVERY 6 MONTHS DURING THE FIRST YEAR OF OPERATION. ADJUST THE INSPECTION INTERVAL BASED ON PREVIOUS OBSERVATIONS OF SEDIMENT ACCUMULATION AND HIGH WATER ELEVATIONS.
- 2. CONDUCT JETTING AND VACTORING ANNUALLY OR WHEN INSPECTION SHOWS THAT MAINTENANCE IS NECESSARY.

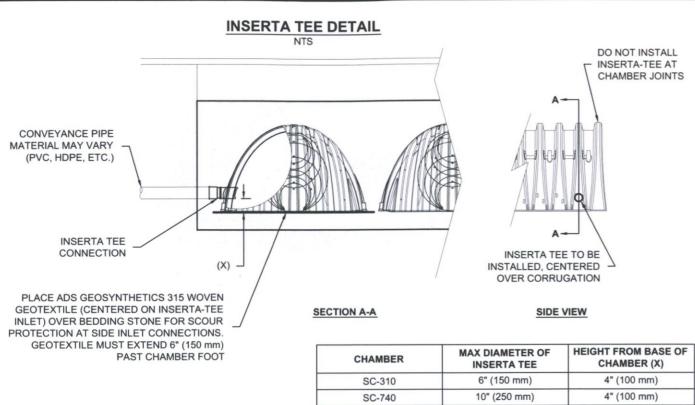


at Miller Rd Scottsdale, 07/06/2018 Storm

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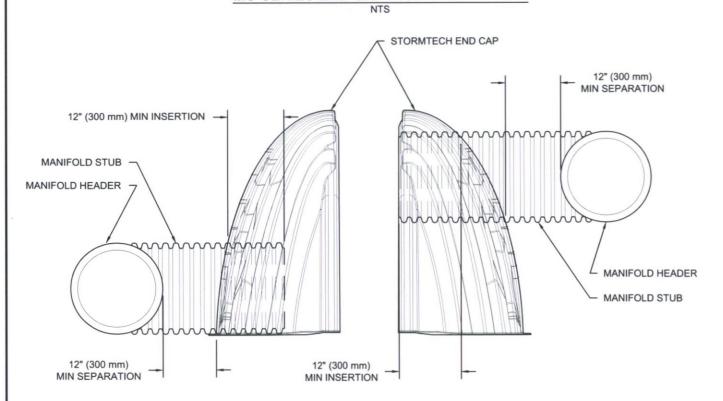
and



CHAMBER	MAX DIAMETER OF INSERTA TEE	CHAMBER (X)
SC-310	6" (150 mm)	4" (100 mm)
SC-740	10" (250 mm)	4" (100 mm)
DC-780	10" (250 mm)	4" (100 mm)
MC-3500	12" (300 mm)	6" (150 mm)
MC-4500	12" (300 mm)	8" (200 mm)
	NGS AVAILABLE FOR SDR 2 NT WELD, N-12, HP STORM,	

PART NUMBERS WILL VARY BASED ON INLET PIPE MATERIALS. CONTACT STORMTECH FOR MORE INFORMATION.

MC-SERIES END CAP INSERTION DETAIL



NOTE: MANIFOLD STUB MUST BE LAID HORIZONTAL FOR A PROPER FIT IN END CAP OPENING.

MC-3500 TECHNICAL SPECIFICATION 86.0" (2184 mm) VALLEY CREST STIFFENING RIB **INSTALLED CREST** STIFFENING RIB LOWER JOINT CORRUGATION UPPER JOINT CORRUGATION BUILD ROW IN THIS DIRECTION ⇒ 90.0" (2286 mm) ACTUAL LENGTH 45.0" 45.0" (1143 mm (1143 mm) 22.5" (571 mm) INSTALLED 77.0" 77.0" (1956 mm) (1956 mm) NOMINAL CHAMBER SPECIFICATIONS SIZE (W X H X INSTALLED LENGTH) 77.0" X 45.0" X 86.0" (1956 mm X 1143 mm X 2184 mm) 109.9 CUBIC FEET CHAMBER STORAGE (3.11 m³) MINIMUM INSTALLED STORAGE* 178.9 CUBIC FEET (5.06 m³) 135.0 lbs. WEIGHT (61.2 kg) 25.7" NOMINAL END CAP SPECIFICATIONS (653 mm) 77.0" X 45.0" X 22.5" (1956 mm X 1143 mm X 571 mm) SIZE (W X H X INSTALLED LENGTH) END CAP STORAGE 14.9 CUBIC FEET (0.42 m³)

(1.30 m³)

(22.7 kg)

*ASSUMES 12" (305 mm) STONE ABOVE, 9" (229 mm) STONE FOUNDATION AND BETWEEN CHAMBERS, 12" (305 mm) STONE PERIMETER IN FRONT OF END CAPS AND 40% STONE POROSITY

50.0 lbs.

46.0 CUBIC FEET

STUBS AT BOTTOM OF END CAP FOR PART NUMBERS ENDING WITH "B"

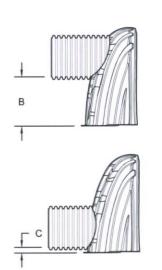
PART#	STUB	В	С
MC3500IEPP06T	6" (4E0 mm)	33.21" (844 mm)	
MC3500IEPP06B	6" (150 mm)		0.66" (17 mm)
MC3500IEPP08T	0" (200)	31.16" (791 mm)	
MC3500IEPP08B	8" (200 mm)		0.81" (21 mm)
MC3500IEPP10T	10" (2E0 mm)	29.04" (738 mm)	
MC3500IEPP10B	10" (250 mm)		0.93" (24 mm)
MC3500IEPP12T MC3500IEPP12B	12" (200 mm)	26.36" (670 mm)	
	12" (300 mm)		1.35" (34 mm)
MC3500IEPP15T	45" /275 mm	23.39" (594 mm)	
MC3500IEPP15B	15" (375 mm)		1.50" (38 mm)
MC3500IEPP18TC	40" (4E0 mm)	20.03" (509 mm)	
MC3500IEPP18BC	18" (450 mm)		1.77" (45 mm)
MC3500IEPP24TC	24" (600)	14.48" (368 mm)	
MC3500IEPP24BC	24" (600 mm)		2.06" (52 mm)
MC3500IEPP30BC	30" (750 mm)		

NOTE: ALL DIMENSIONS ARE NOMINAL

MINIMUM INSTALLED STORAGE*

CUSTOM PRECORED INVERTS ARE AVAILABLE UPON REQUEST. INVENTORIED MANIFOLDS INCLUDE 12-24" (300-600 mm) SIZE ON SIZE AND 15-48" (375-1200 mm) ECCENTRIC MANIFOLDS. CUSTOM INVERT LOCATIONS ON THE MC-3500 END CAP CUT IN THE FIELD ARE NOT RECOMMENDED FOR PIPE SIZES GREATER THAN 10" (250 mm)

THE INVERT LOCATION IN COLUMN 'B' ARE THE HIGHTEST POSSIBLE FOR THE PIPE SIZE.



Townhomes at Miller Rd and

Scottsdale, Arizona

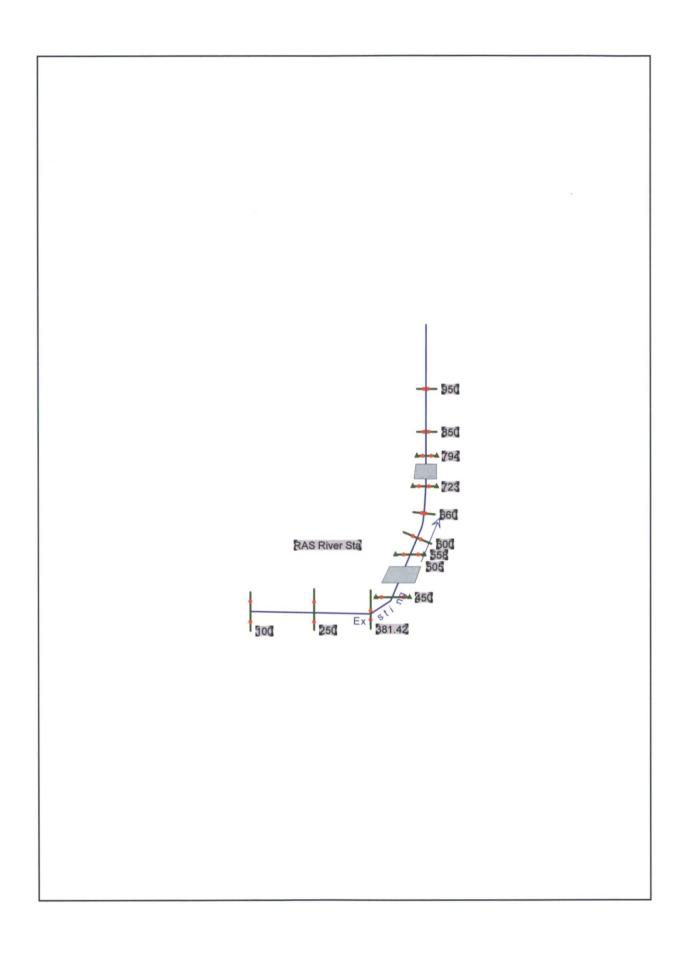
BD

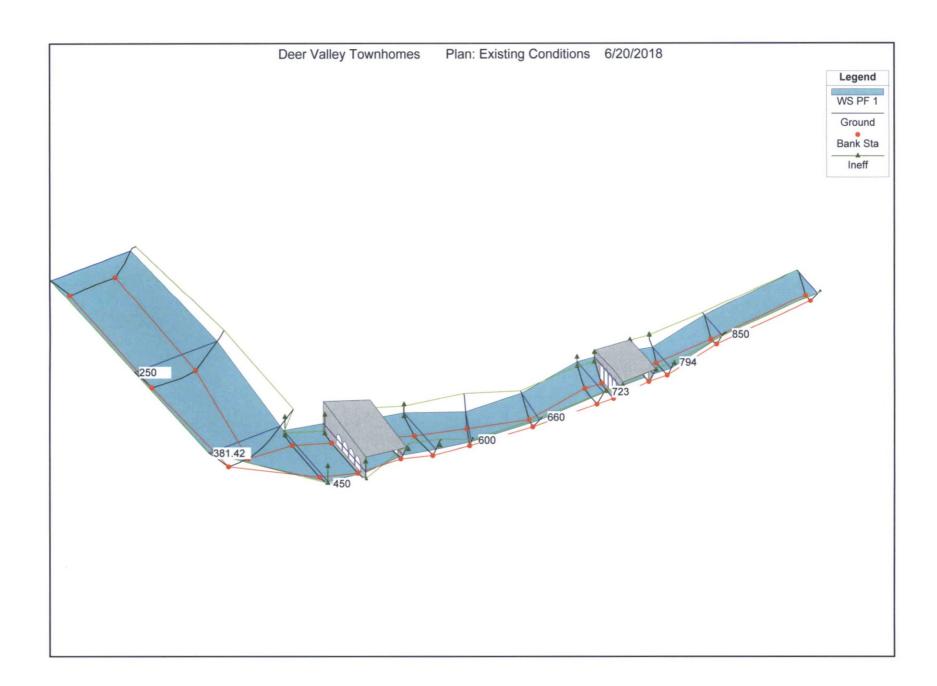
07/06/2018

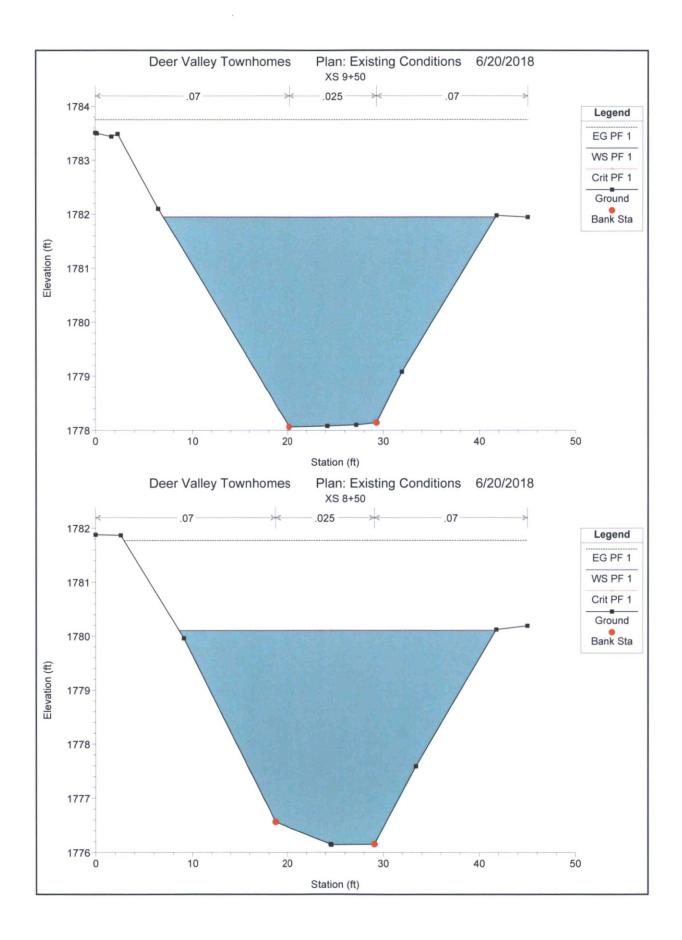
SHEET 5 OF 5

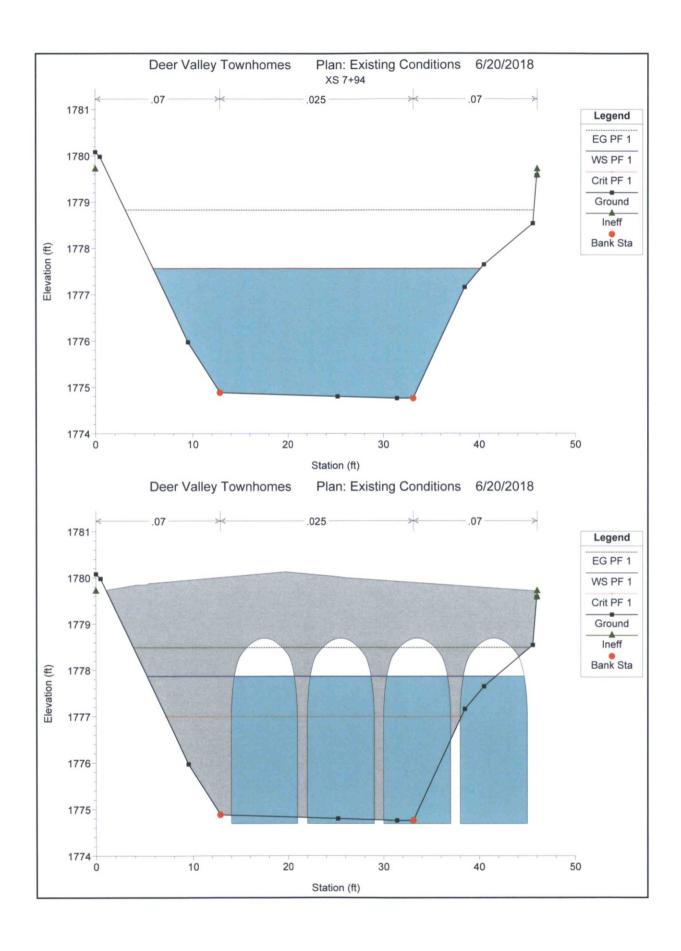
Appendix E

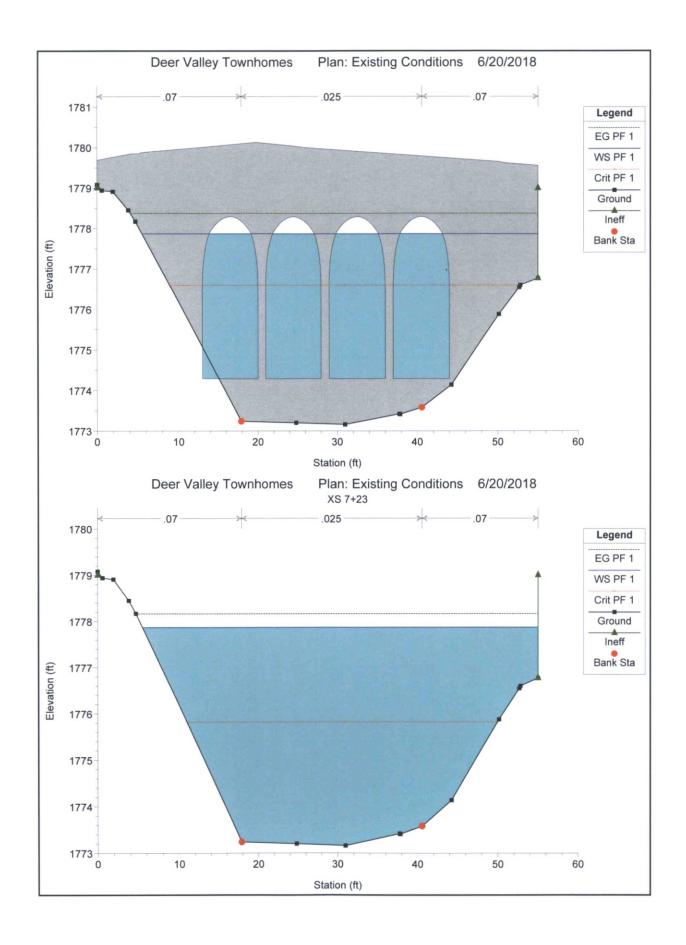
HEC-RAS Output

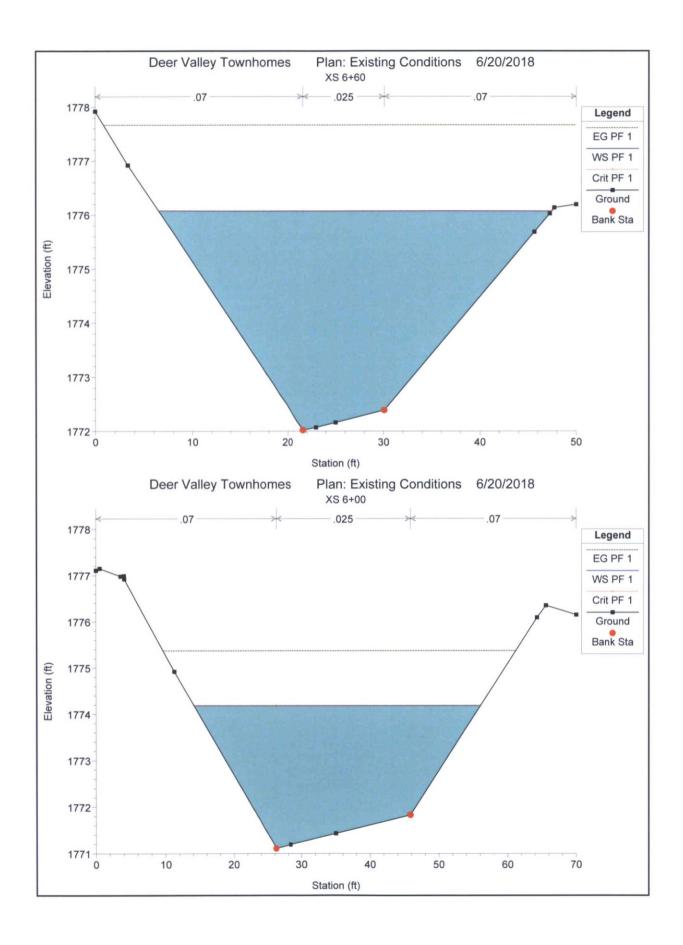


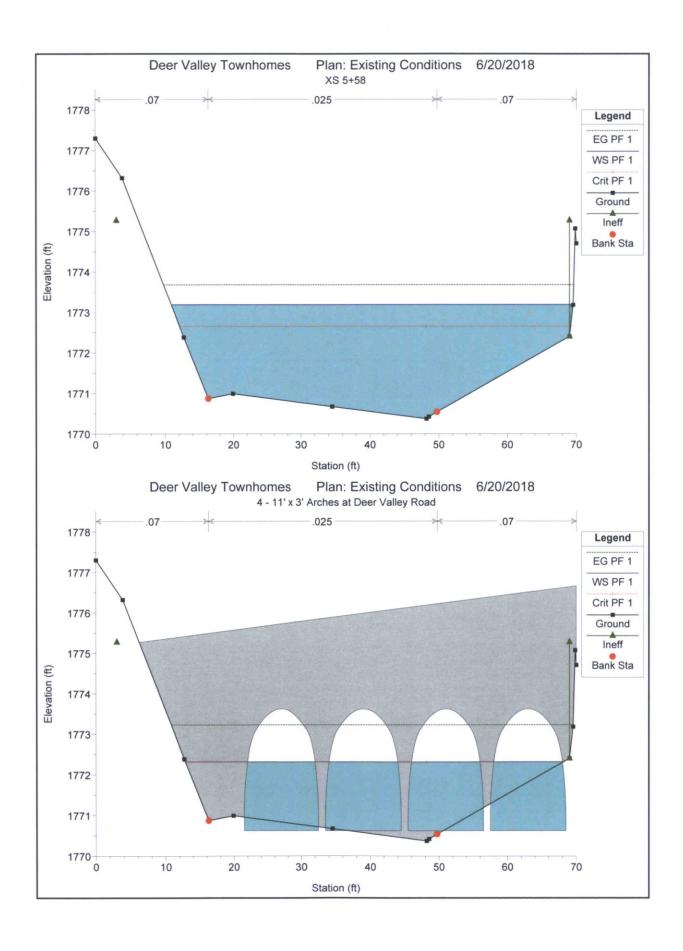


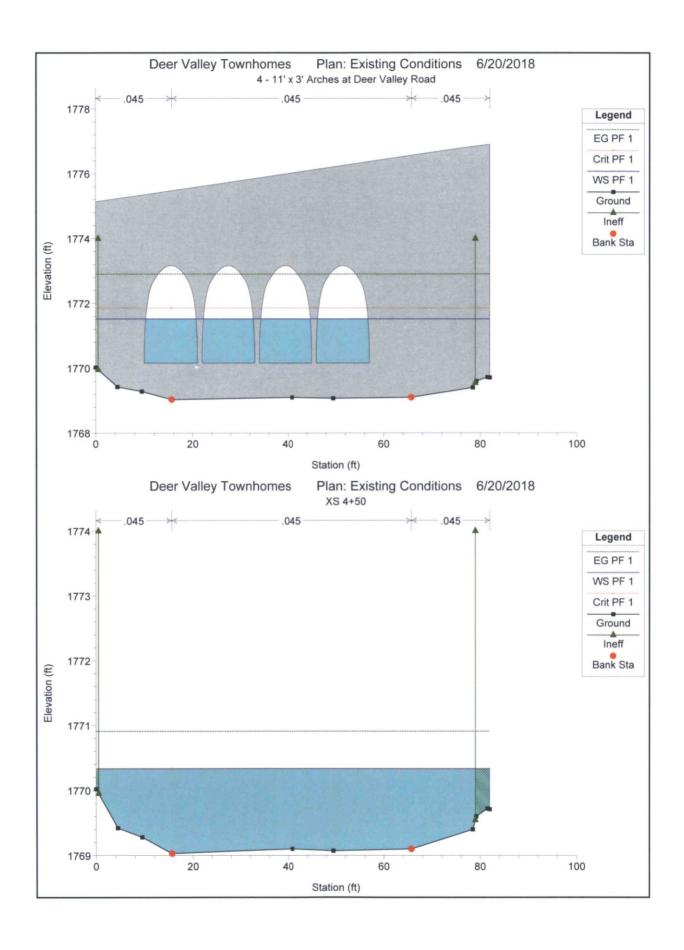


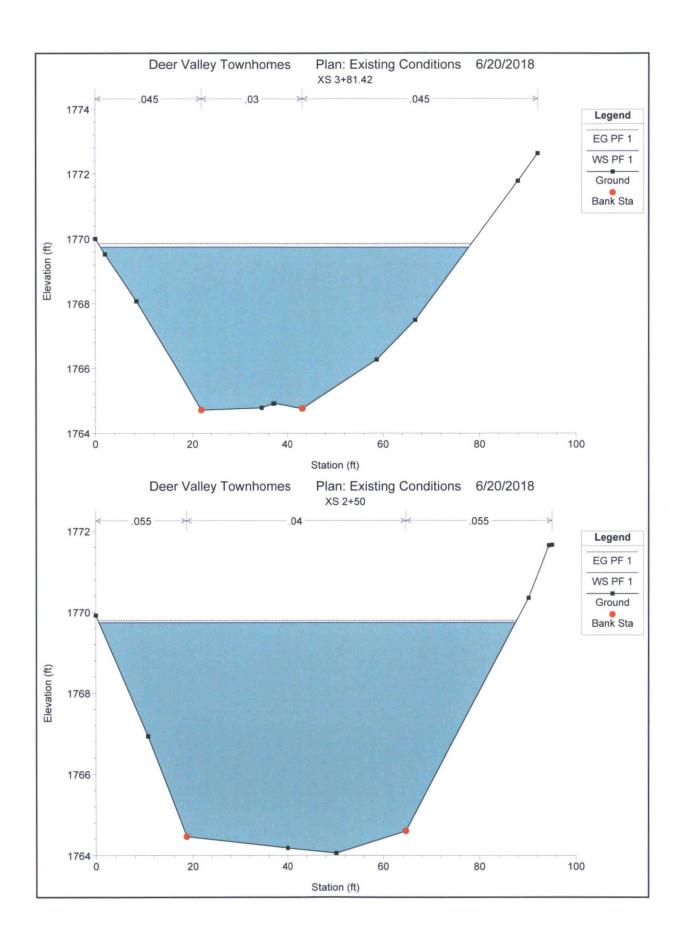


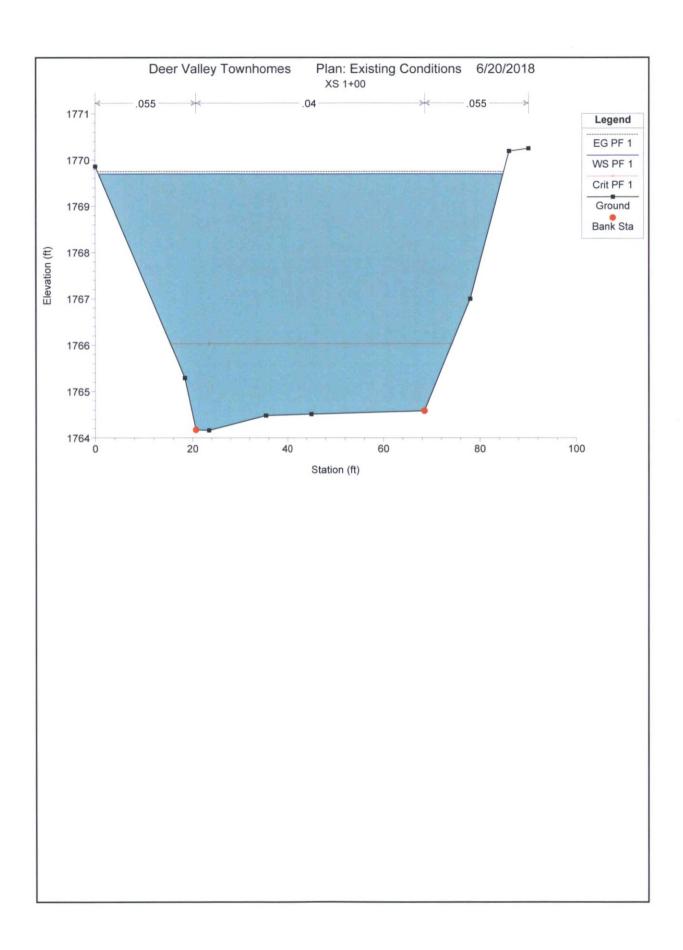












HEC-RAS Plan: EX COND River: Existing Reach: RAS River Sta Profile: PF 1

Reach	River Sta	Profile	Q Total	Min Ch El	W.S. Elev	Crit W.S.	E.G. Elev	E.G. Slope	Vel Chnl	Flow Area	Top Width	Froude # Chl
			(cfs)	(ft)	(ft)	(ft)	(ft)	(ft/ft)	(ft/s)	(sq ft)	(ft)	
RAS River Sta	950	PF 1	557.00	1778.06	1781.95	1781.95	1783.76	0.006950	12.20	83.71	34.73	1.09
RAS River Sta	850	PF 1	557.00	1776.14	1780.11	1780.11	1781.77	0.006141	11.42	82.10	33.14	1.03
RAS River Sta	794	PF 1	557.00	1774.76	1777.57	1777.57	1778.83	0.006384	9.32	74.73	34.23	0.99
RAS River Sta	757		Culvert									
RAS River Sta	723	PF 1	557.00	1773.16	1777.87	1775.82	1778.17	0.000801	4.66	171.75	49.51	0.38
RAS River Sta	660	PF 1	557.00	1772.02	1776.08	1776.08	1777.67	0.006634	11.94	95.62	40.98	1.07
RAS River Sta	600	PF 1	557.00	1771.11	1774.18	1774.18	1775.37	0.006423	9.26	83.85	41.91	0.99
RAS River Sta	558	PF 1	557.00	1770.37	1773.19	1772.66	1773.68	0.002940	5.93	123.01	58.66	0.66
RAS River Sta	505		Culvert									
RAS River Sta	450	PF 1	557.00	1769.03	1770.33	1770.33	1770.91	0.026927	6.31	92.00	82.00	0.99
RAS River Sta	381.42	PF 1	557.00	1764.71	1769.75		1769.86	0.000495	3.20	258.18	76.76	0.25
RAS River Sta	250	PF 1	557.00	1764.05	1769.74		1769.79	0.000265	1.88	356.65	86.83	0.14
RAS River Sta	100	PF 1	557.00	1764.16	1769.70	1766.03	1769.75	0.000285	1.89	347.50	84.08	0.15

Plan: EX COND	Existing	RAS River Sta	RS: 950	Profile: PF 1
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E.G. Elev (ft)	1783.76	Element	Left OB	Channel	Right OB
Vel Head (ft)	1.80	Wt. n-Val.	0.070	0.025	0.070
W.S. Elev (ft)	1781.95	Reach Len. (ft)	100.00	100.00	100.00
Crit W.S. (ft)	1781.95	Flow Area (sq ft)	25.70	35.18	22.83
E.G. Slope (ft/ft)	0.006950	Area (sq ft)	25.70	35.18	22.83
Q Total (cfs)	557.00	Flow (cfs)	68.92	429.12	58.96
Top Width (ft)	34.73	Top Width (ft)	13.21	9.11	12.41
Vel Total (ft/s)	6.65	Avg. Vel. (ft/s)	2.68	12.20	2.58
Max Chl Dpth (ft)	3.89	Hydr. Depth (ft)	1.95	3.86	1.84
Conv. Total (cfs)	6681.5	Conv. (cfs)	826.7	5147.5	707.2
Length Wtd. (ft)	100.00	Wetted Per. (ft)	13.77	9.11	12.98
Min Ch El (ft)	1778.06	Shear (lb/sq ft)	0.81	1.68	0.76
Alpha	2.62	Stream Power (lb/ft s)	2.17	20.44	1.97
Frctn Loss (ft)	0.65	Cum Volume (acre-ft)	0.52	2.05	0.69
C & E Loss (ft)	0.04	Cum SA (acres)	0.28	0.57	0.35

Plan: EX COND Existing RAS River Sta RS: 850 Profile: PF 1

E.G. Elev (ft)	1781.77	Element	Left OB	Channel	Right OB
Vel Head (ft)	1.67	Wt. n-Val.	0.070	0.025	0.070
W.S. Elev (ft)	1780.11	Reach Len. (ft)	56.00	56.00	56.00
Crit W.S. (ft)	1780.11	Flow Area (sq ft)	17.87	39.78	24.45
E.G. Slope (ft/ft)	0.006141	Area (sq ft)	17.87	39.78	24.45
Q Total (cfs)	557.00	Flow (cfs)	41.68	454.08	61.24
Top Width (ft)	33.14	Top Width (ft)	10.15	10.35	12.63
Vel Total (ft/s)	6.78	Avg. Vel. (ft/s)	2.33	11.42	2.50
Max Chl Dpth (ft)	3.97	Hydr. Depth (ft)	1.76	3.84	1.94
Conv. Total (cfs)	7108.0	Conv. (cfs)	531.9	5794.6	781.5
Length Wtd. (ft)	56.00	Wetted Per. (ft)	10.76	10.37	13.24
Min Ch El (ft)	1776.14	Shear (lb/sq ft)	0.64	1.47	0.71
Alpha	2.33	Stream Power (lb/ft s)	1.49	16.79	1.77
Frctn Loss (ft)	0.35	Cum Volume (acre-ft)	0.47	1.97	0.64
C & E Loss (ft)	0.12	Cum SA (acres)	0.25	0.55	0.32

Plan: EX COND Existing RAS River Sta RS: 794 Profile: PF 1

E.G. Flev (ft) 1778 83 Element Left OB Channel Right OB

E.G. Elev (ft)	1778.83	Element	Left OB	Channel	Right OB
Vel Head (ft)	1.26	Wt. n-Val.	0.070	0.025	0.070
W.S. Elev (ft)	1777.57	Reach Len. (ft)	71.00	71.00	71.00
Crit W.S. (ft)	1777.57	Flow Area (sq ft)	10.07	55.69	8.97
E.G. Slope (ft/ft)	0.006384	Area (sq ft)	10.07	55.69	8.97
Q Total (cfs)	557.00	Flow (cfs)	20.86	519.13	17.01
Top Width (ft)	34.23	Top Width (ft)	6.96	20.25	7.02
Vel Total (ft/s)	7.45	Avg. Vel. (ft/s)	2.07	9.32	1.90
Max Chl Dpth (ft)	2.81	Hydr. Depth (ft)	1.45	2.75	1.28
Conv. Total (cfs)	6971.1	Conv. (cfs)	261.0	6497.2	212.9
Length Wtd. (ft)	71.00	Wetted Per. (ft)	7.47	20.25	7.59
Min Ch El (ft)	1774.76	Shear (lb/sq ft)	0.54	1.10	0.47
Alpha	1.46	Stream Power (lb/ft s)	1.11	10.22	0.89
Frctn Loss (ft)		Cum Volume (acre-ft)	0.46	1.91	0.62
C & E Loss (ft)		Cum SA (acres)	0.24	0.53	0.31

Plan: EX COND	Existing	RAS River Sta	RS: 723	Profile: PF 1
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E.G. Elev (ft)	1778.17	Element	Left OB	Channel	Right OB
Vel Head (ft)	0.30	Wt. n-Val.	0.070	0.025	0.070
W.S. Elev (ft)	1777.87	Reach Len. (ft)	63.00	63.00	63.00
Crit W.S. (ft)	1775.82	Flow Area (sq ft)	28.70	104.47	38.58
E.G. Slope (ft/ft)	0.000801	Area (sq ft)	28.70	104.47	38.58
Q Total (cfs)	557.00	Flow (cfs)	28.89	486.32	41.80
Top Width (ft)	49.51	Top Width (ft)	12.40	22.68	14.43
Vel Total (ft/s)	3.24	Avg. Vel. (ft/s)	1.01	4.66	1.08
Max Chl Dpth (ft)	4.71	Hydr. Depth (ft)	2.32	4.61	2.67
Conv. Total (cfs)	19681.9	Conv. (cfs)	1020.7	17184.2	1476.9
Length Wtd. (ft)	63.00	Wetted Per. (ft)	13.23	22.69	15.93
Min Ch El (ft)	1773.16	Shear (lb/sq ft)	0.11	0.23	0.12
Alpha	1.81	Stream Power (lb/ft s)	0.11	1.07	0.13
Frctn Loss (ft)	0.11	Cum Volume (acre-ft)	0.46	1.85	0.62
C & E Loss (ft)	0.39	Cum SA (acres)	0.23	0.49	0.29

Plan: EX COND Existing RAS River Sta RS: 660 Profile: PF 1

E.G. Elev (ft)	1777.67	Element	Left OB	Channel	Right OB
Vel Head (ft)	1.59	Wt. n-Val.	0.070	0.025	0.070
W.S. Elev (ft)	1776.08	Reach Len. (ft)	60.00	60.00	60.00
Crit W.S. (ft)	1776.08	Flow Area (sq ft)	30.73	32.77	32.12
E.G. Slope (ft/ft)	0.006634	Area (sq ft)	30.73	32.77	32.12
Q Total (cfs)	557.00	Flow (cfs)	83.21	391.42	82.37
Top Width (ft)	40.98	Top Width (ft)	15.14	8.45	17.39
Vel Total (ft/s)	5.83	Avg. Vel. (ft/s)	2.71	11.94	2.56
Max Chl Dpth (ft)	4.06	Hydr. Depth (ft)	2.03	3.88	1.85
Conv. Total (cfs)	6838.4	Conv. (cfs)	1021.5	4805.5	1011.3
Length Wtd. (ft)	60.00	Wetted Per. (ft)	15.68	8.46	17.78
Min Ch El (ft)	1772.02	Shear (lb/sq ft)	0.81	1.60	0.75
Alpha	3.01	Stream Power (lb/ft s)	2.20	19.17	1.92
Frctn Loss (ft)	0.39	Cum Volume (acre-ft)	0.41	1.75	0.57
C & E Loss (ft)	0.12	Cum SA (acres)	0.21	0.47	0.27

Plan: EX COND Existing RAS River Sta RS: 600 Profile: PF 1

E.G. Elev (ft)	1775.37	Element	Left OB	Channel	Right OB
Vel Head (ft)	1.19	Wt. n-Val.	0.070	0.025	0.070
W.S. Elev (ft)	1774.18	Reach Len. (ft)	42.00	42.00	42.00
Crit W.S. (ft)	1774.18	Flow Area (sq ft)	18.62	53.27	11.96
E.G. Slope (ft/ft)	0.006423	Area (sq ft)	18.62	53.27	11.96
Q Total (cfs)	557.00	Flow (cfs)	41.32	493.39	22.29
Top Width (ft)	41.91	Top Width (ft)	12.12	19.63	10.17
Vel Total (ft/s)	6.64	Avg. Vel. (ft/s)	2.22	9.26	1.86
Max Chl Dpth (ft)	3.07	Hydr. Depth (ft)	1.54	2.71	1.18
Conv. Total (cfs)	6950.0	Conv. (cfs)	515.5	6156.4	278.1
Length Wtd. (ft)	42.00	Wetted Per. (ft)	12.50	19.64	10.43
Min Ch El (ft)	1771.11	Shear (lb/sq ft)	0.60	1.09	0.46
Alpha	1.73	Stream Power (lb/ft s)	1.33	10.07	0.86
Frctn Loss (ft)	0.18	Cum Volume (acre-ft)	0.38	1.69	0.54
C & E Loss (ft)	0.21	Cum SA (acres)	0.19	0.45	0.25

Plan: EX COND Existing	RAS River Sta	RS: 558	Profile: PF 1
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E.G. Elev (ft)	1773.68	Element	Left OB	Channel	Right OB
Vel Head (ft)	0.49	Wt. n-Val.	0.070	0.025	0.070
W.S. Elev (ft)	1773.19	Reach Len. (ft)	108.00	108.00	108.00
Crit W.S. (ft)	1772.66	Flow Area (sq ft)	6.38	83.47	33.16
E.G. Slope (ft/ft)	0.002940	Area (sq ft)	6.38	83.47	33.38
Q Total (cfs)	557.00	Flow (cfs)	7.74	494.60	54.67
Top Width (ft)	58.66	Top Width (ft)	5.42	33.46	19.78
Vel Total (ft/s)	4.53	Avg. Vel. (ft/s)	1.21	5.93	1.65
Max Chl Dpth (ft)	2.82	Hydr. Depth (ft)	1.18	2.49	1.72
Conv. Total (cfs)	10273.0	Conv. (cfs)	142.7	9122.1	1008.3
Length Wtd. (ft)	108.00	Wetted Per. (ft)	5.90	33.48	19.34
Min Ch El (ft)	1770.37	Shear (lb/sq ft)	0.20	0.46	0.31
Alpha	1.53	Stream Power (lb/ft s)	0.24	2.71	0.52
Frctn Loss (ft)		Cum Volume (acre-ft)	0.37	1.62	0.51
C & E Loss (ft)		Cum SA (acres)	0.18	0.42	0.24

Plan: EX COND Existing RAS River Sta RS: 450 Profile: PF 1

E.G. Elev (ft)	1770.91	Element	Left OB	Channel	Right OB
Vel Head (ft)	0.58	Wt. n-Val.	0.045	0.045	0.045
W.S. Elev (ft)	1770.33	Reach Len. (ft)	68.58	68.58	68.58
Crit W.S. (ft)	1770.33	Flow Area (sq ft)	14.67	63.09	14.24
E.G. Slope (ft/ft)	0.026927	Area (sq ft)	14.84	63.09	16.25
Q Total (cfs)	557.00	Flow (cfs)	77.94	398.27	80.79
Top Width (ft)	82.00	Top Width (ft)	15.57	50.17	16.26
Vel Total (ft/s)	6.05	Avg. Vel. (ft/s)	5.31	6.31	5.67
Max Chl Dpth (ft)	1.30	Hydr. Depth (ft)	0.97	1.26	1.07
Conv. Total (cfs)	3394.4	Conv. (cfs)	475.0	2427.1	492.4
Length Wtd. (ft)	68.58	Wetted Per. (ft)	15.11	50.17	13.28
Min Ch El (ft)	1769.03	Shear (lb/sq ft)	1.63	2.11	1.80
Alpha	1.01	Stream Power (lb/ft s)	8.67	13.34	10.22
Frctn Loss (ft)	0.11	Cum Volume (acre-ft)	0.37	1.54	0.51
C & E Loss (ft)	0.02	Cum SA (acres)	0.15	0.32	0.19

Plan: EX COND Existing RAS River Sta RS: 381.42 Profile: PF 1

E.G. Elev (ft)	1769.86	Element	Left OB	Channel	Right OB
Vel Head (ft)	0.11	Wt. n-Val.	0.045	0.030	0.045
W.S. Elev (ft)	1769.75	Reach Len. (ft)	131.42	131.42	131.42
Crit W.S. (ft)		Flow Area (sq ft)	51.28	105.87	101.04
E.G. Slope (ft/ft)	0.000495	Area (sq ft)	51.28	105.87	101.04
Q Total (cfs)	557.00	Flow (cfs)	67.45	339.17	150.38
Top Width (ft)	76.76	Top Width (ft)	20.79	21.34	34.63
Vel Total (ft/s)	2.16	Avg. Vel. (ft/s)	1.32	3.20	1.49
Max Chl Dpth (ft) 5.04		Hydr. Depth (ft)	2.47	4.96	2.92
Conv. Total (cfs)	25044.7	Conv. (cfs)	3032.6	15250.4	6761.7
Length Wtd. (ft)	131.42	Wetted Per. (ft)	21.39	21.35	35.02
Min Ch El (ft)	1764.71	Shear (lb/sq ft)	0.07	0.15	0.09
Alpha	1.52	Stream Power (lb/ft s)	0.10	0.49	0.13
Frctn Loss (ft)	0.05	Cum Volume (acre-ft)	0.31	1.40	0.42
C & E Loss (ft)	0.02	Cum SA (acres)	0.12	0.26	0.15

Plan: EX COND Existing RAS River Sta RS: 250 Profile: PF 1

E.G. Elev (ft)	1769.79	Element	Left OB	Channel	Right OB
Vel Head (ft) 0.05		Wt. n-Val.	0.055	0.040	0.055
W.S. Elev (ft)	1769.74	Reach Len. (ft)	150.00	150.00	150.00
Crit W.S. (ft)		Flow Area (sq ft)	46.48	251.72	58.45
E.G. Slope (ft/ft)	0.000265	Area (sq ft)	46.48	251.72	58.45
Q Total (cfs)	557.00	Flow (cfs)	37.36	472.19	47.45
Top Width (ft)	86.83	Top Width (ft)	18.04	46.05	22.73
Vel Total (ft/s)	1.56	Avg. Vel. (ft/s)	0.80	1.88	0.81
Max Chl Dpth (ft)	5.69	Hydr. Depth (ft)	2.58	5.47	2.57
Conv. Total (cfs)	34220.9	Conv. (cfs)	2295.5	29010.3	2915.1
Length Wtd. (ft)	150.00	Wetted Per. (ft)	18.80	46.06	23.31
Min Ch El (ft)	1764.05	Shear (lb/sq ft)	0.04	0.09	0.04
Alpha	1.26	Stream Power (lb/ft s)	0.03	0.17	0.03
Frctn Loss (ft)	0.04	Cum Volume (acre-ft)	0.17	0.86	0.18
C & E Loss (ft)	0.00	Cum SA (acres)	0.07	0.16	0.07

Plan: EX COND Existing RAS River Sta RS: 100 Profile: PF 1

E.G. Elev (ft)	1769.75	Element	Left OB	Channel	Right OB
Vel Head (ft)	0.05	Wt. n-Val.	0.055	0.040	0.055
W.S. Elev (ft)	1769.70	Reach Len. (ft)			
Crit W.S. (ft)	1766.03	Flow Area (sq ft)	50.67	250.58	46.25
E.G. Slope (ft/ft)	0.000285	Area (sq ft)	50.67	250.58	46.25
Q Total (cfs)	557.00	Flow (cfs)	41.79	474.22	41.00
Top Width (ft)	84.08	Top Width (ft)	20.05	47.79	16.25
Vel Total (ft/s)	1.60	Avg. Vel. (ft/s)	0.82	1.89	0.89
Max Chl Dpth (ft)	5.54	Hydr. Depth (ft)	2.53	5.24	2.85
Conv. Total (cfs)	32996.4	Conv. (cfs)	2475.3	28092.5	2428.6
Length Wtd. (ft)		Wetted Per. (ft)	20.84	47.79	17.07
Min Ch El (ft)	1764.16	Shear (lb/sq ft)	0.04	0.09	0.05
Alpha	1.23	Stream Power (lb/ft s)	0.04	0.18	0.04
Frctn Loss (ft)		Cum Volume (acre-ft)			
C & E Loss (ft)		Cum SA (acres)			

Plan: EX COND Existi	ng RAS Riv	er Sta RS: 757 Culv Grou	p: Culvert #1	Profile: PF
Q Culv Group (cfs)	557.00	Culv Full Len (ft)		
# Barrels	4	Culv Vel US (ft/s)	6.32	
Q Barrel (cfs)	139.25	Culv Vel DS (ft/s)	5.70	
E.G. US. (ft)	1778.80	Culv Inv El Up (ft)	1774.69	
W.S. US. (ft)	1777.57	Culv Inv El Dn (ft)	1774.29	
E.G. DS (ft)	1778.17	Culv Frctn Ls (ft)	0.11	
W.S. DS (ft)	1777.87	Culv Exit Loss (ft)	0.21	
Delta EG (ft)	0.63	Culv Entr Loss (ft)	0.31	
Delta WS (ft)	0.31	Q Weir (cfs)		
E.G. IC (ft)	1778.56	Weir Sta Lft (ft)		
E.G. OC (ft)	1778.80	Weir Sta Rgt (ft)		
Culvert Control	Outlet	Weir Submerg		
Culv WS Inlet (ft)	1777.87	Weir Max Depth (ft)		
Culv WS Outlet (ft)	1777.87	Weir Avg Depth (ft)		
Culv Nml Depth (ft)	2.18	Weir Flow Area (sq ft)		
Culv Crt Depth (ft)	2.31	Min El Weir Flow (ft)	1779.72	

Plan: EX COND Existing	ng RAS Riv	er Sta RS: 505 Culv Grou	p: Culvert #
Q Culv Group (cfs)	557.00	Culv Full Len (ft)	
# Barrels	4	Culv Vel US (ft/s)	7.66
Q Barrel (cfs)	139.25	Culv Vel DS (ft/s)	9.43
E.G. US. (ft)	1773.68	Culv Inv El Up (ft)	1770.62
W.S. US. (ft)	1773.19	Culv Inv El Dn (ft)	1770.16
E.G. DS (ft)	1770.91	Culv Frctn Ls (ft)	0.32
W.S. DS (ft)	1770.33	Culv Exit Loss (ft)	2.00
Delta EG (ft)	2.78	Culv Entr Loss (ft)	0.46
Delta WS (ft)	2.86	Q Weir (cfs)	
E.G. IC (ft)	1773.39	Weir Sta Lft (ft)	
E.G. OC (ft)	1773.68	Weir Sta Rgt (ft)	
Culvert Control	Outlet	Weir Submerg	
Culv WS Inlet (ft)	1772.32	Weir Max Depth (ft)	
Culv WS Outlet (ft)	1771.52	Weir Avg Depth (ft)	
Culv Nml Depth (ft)	1.27	Weir Flow Area (sq ft)	
Culv Crt Depth (ft)	1.70	Min El Weir Flow (ft)	1775.28

Profile: PF 1

LISTEN DESIGN PLAN BUILD

Preliminary Basis of Design Report Water

Deer Valley Townhomes

NWC of Miller Road & Deer Valley Road

City of Scottsdale

Maricopa County, Arizona

TSC Project No. 0800

August 27, 2018

Prepared for:

Beardsley 22, Inc 222 W Linger Lane, Phoenix, AZ 85021



civil engineering • surveying • urban planning

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3.0	Domestic Water Demand Calculations	2
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Appendix A: Fire Flow Test

Appendix B: Preliminary Grading & Drainage Plan

Appendix C: IFC - Appendix B

1.0 Introduction

The proposed Deer Valley Townhomes development (Project) consists of attached townhomes split between three (3) buildings on a one acre parcel. The Site is defined by the parcel boundary for APN# 212-02-010E and is located at the northwest corner of Miller Road and Deer Valley Road in Scottsdale (see figure 1 below). The current project zoning is PCOC and proposed project zoning is R-3. The site is currently undeveloped and the proposed development will be constructed all at once and will not be phased.

The purpose of this report is to evaluate the Site's existing and proposed water and fire infrastructure to determine if adequate supply is available. This report takes into consideration the projected water demand, fire demand, and its impact. The Project will be designed and developed in accordance with the City of Scottsdale amendment to the 2015 International Fire Code, 2018 City of Scottsdale Design Standards & Policies Manual (DSPM), County, and State requirements.



Figure 1: Location Map

2.0 Water System

The Site is a vacant lot with a channel along the east side. There are existing water lines in Deer Valley Road and Miller Road. City quarter section maps show various water lines along Miller Road that continue west on Deer Valley Road, which may be raw water or transmission mains but do not negatively impact the Site. There

appears to be a water tank on the south side of Deer Valley Road. An 8" D.I.P. water line exists in Calistoga Circle within the Arizona Silverado subdivision. This line is located at the northwest corner of the Site with a service line that extends to the site with a blowoff at the end of the line.

A water meter is proposed at the northwest corner of the property within the existing City utility and drainage easement shown on the Arizona Silverado Final Plat. The meter size is estimated at 1-½", but will need to be confirmed during the construction document phase. A 1-½" domestic water line is estimated at this time to service the Site, with individual connections to each home. During final design, it may be determined that each structure requires one domestic service not one per home. Considering the residual pressure of 96 psi along Deer Valley Road, a pressure reducing valve may be required for the domestic supply. See **Appendix A** for flow test results.

3.0 <u>Domestic Water Demand Calculations</u>

Unit Count = 9

Average Day Flow (ADF) = $9 \times 227.6 \text{ gpd/unit} = 2,048.4 \text{ gpd} = 2,048.4 \text{ gpd/1440(min/day)} = 1.42 \text{ gpm}$

Maximum Day Flow (MDF) = ADF x 2.0 = 1.42 gpm x 2.0 = 2.84 gpm

Peak Hour Flow (PHF) = ADF x 3.5 = 1.42 gpm x 3.5 = 4.97 gpm

*ADF based on DSPM figure 6-1.2

*MDF and PHF based on DSPM section 6-1.404.B

4.0 Fire Flow Calculations

The Project falls within the City of Scottsdale service boundary in Pressure Zone 6. There is an existing hydrant south of the Site at the northwest corner of the headwall for the culvert under Deer Valley Road. This hydrant is to be relocated west of the proposed driveway into the site. An additional hydrant is proposed at the northwest corner to meet hose lay requirement for the northernmost structure.

According to DSPM Section 6-1.501, a minimum system fire flow of 1,500 gpm is required for commercial, industrial, and multi-family residential developments. The largest structure on site has a footprint of 6,100 sf and does not contain fire walls. Upon final determination of the building construction type being classified as V-A, **Appendix B** of the 2015 International Fire Code indicates the fire flow demand is 1,500 for a duration of two hours. The flow tests provided in **Appendix A** show that the supply meets the demand requirements.



APPENDIX A

FIRE FLOW TEST



Flow Test Summary

Project Name:

EJFT 18159

Project Address:

7601 E Deer Valley Rd, Scottsdale, AZ 85255

Date of Flow Test:

2018-07-09

Time of Flow Test:

7:30 AM

Data Reliable Until:

2019-01-09

Conducted By:

Tayler Lynch & Eder Cueva (EJ Flow Tests) 602.999.7637

Witnessed By:

Jim Demarbiex (City of Scottsdale) 602.541.0586

City Forces Contacted:

City of Scottsdale (602.228.2187)

Permit Number:

C55801

Note

Scottsdale requires a max static pressure of 72 psi for safety factor

Raw Flow Test Data

Static Pressure:

100.0 PSI

Residual Pressure:

96.0 PSI

Flowing GPM:

2,455

GPM @ 20 PSI:

12,378

Data with a 28 PSI Safety Factor

Static Pressure:

72.0 PSI

Residual Pressure:

68.0 PSI

Flowing GPM:

2,455

GPM @ 20 PSI:

9,809

Hydrant F₁

Pitot Pressure (1):

52 PSI

Coefficient of Discharge (1):

0.9

Hydrant Orifice Diameter (1):

2.5 inches

PSI

Pitot Pressure (2):

55 0.9

Coefficient of Discharge (2): Hydrant Orifice Diameter (2):

2.5 inches





Static-Residual Hydrant



Flow Hydrant

Distance Between F₁ and R 287 ft (measured linearly)

Static-Residual Elevation 1771 ft (above sea level)

Flow Hydrant (F₁) Elevation 1774 ft (above sea level)

Elevation & distance values are approximate



Flow Test Summary

Static-Residual Hydrant



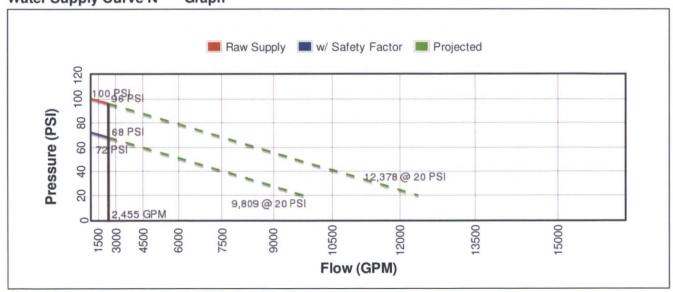
Flow Hydrant (only hydrant F1 shown for clarity)



Approximate Project Site

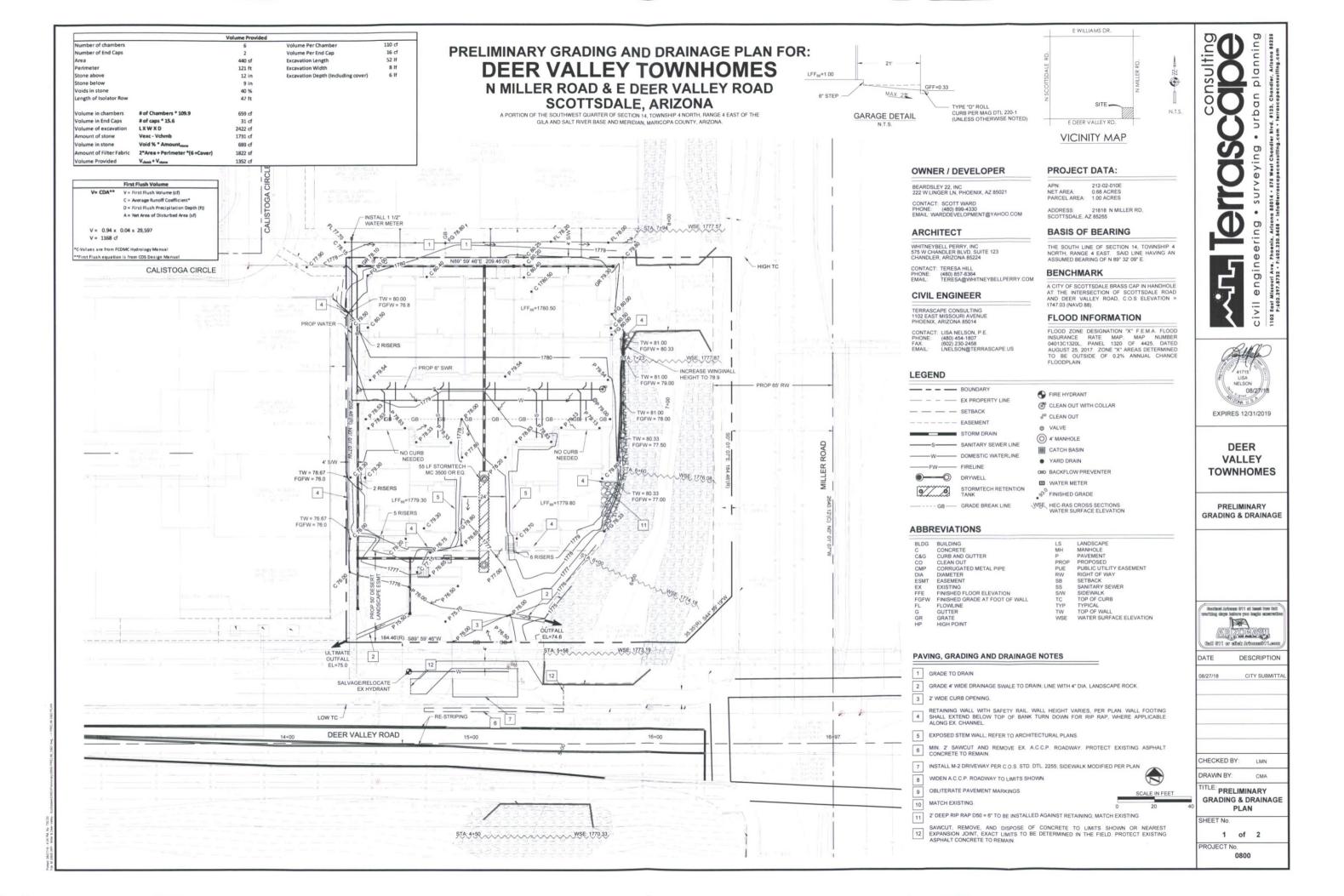


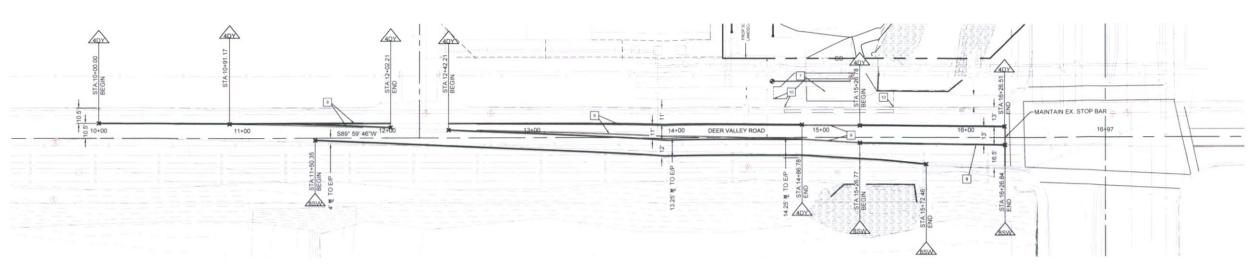
Water Supply Curve N^{1.85} Graph

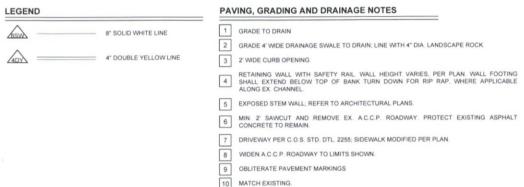


APPENDIX B

PRELIMINARY GRADING & DRAINAGE PLAN







2' DEEP RIP RAP D50 = 6" TO BE INSTALLED AGAINST RETAINING; MATCH EXISTING





DEER VALLEY TOWNHOMES

PRELIMINARY GRADING & DRAINAGE

Genilled Automore 1911 of linear free but sometime deep before you begin asserted on a continue deep before you begin asserted on a continue deep before you begin asserted on a continue of the continue of t

DATE DESCRIPTION

CHECKED BY: LMN

DRAWN BY: CM/

TITLE: PRELIMINARY
GRADING & DRAINAGE
PLAN

SHEET No.

2 of 2 PROJECT No.

SCALE IN FEET

APPENDIX C

IFC - Appendix "B"

APPENDIX B

FIRE-FLOW REQUIREMENTS FOR BUILDINGS

The provisions contained in this appendix are not mandatory unless specifically referenced in the adopting ordinance.

SECTION B101 GENERAL

B101.1 Scope. The procedure for determining fire-flow requirements for buildings or portions of buildings hereafter constructed shall be in accordance with this appendix. This appendix does not apply to structures other than buildings.

SECTION B102 DEFINITIONS

B102.1 Definitions. For the purpose of this appendix, certain terms are defined as follows:

FIRE-FLOW. The flow rate of a water supply, measured at 20 pounds per square inch (psi) (138 kPa) residual pressure, that is available for fire fighting.

FIRE-FLOW CALCULATION AREA. The floor area, in square feet (m²), used to determine the required fire flow.

SECTION B103 MODIFICATIONS

B103.1 Decreases. The fire chief is authorized to reduce the fire-flow requirements for isolated buildings or a group of buildings in rural areas or small communities where the development of full fire-flow requirements is impractical.

B103.2 Increases. The fire chief is authorized to increase the fire-flow requirements where conditions indicate an unusual susceptibility to group fires or conflagrations. An increase shall not be more than twice that required for the building under consideration.

B103.3 Areas without water supply systems. For information regarding water supplies for fire-fighting purposes in rural and suburban areas in which adequate and reliable water supply systems do not exist, the *fire code official* is authorized to utilize NFPA 1142 or the *International Wildland-Urban Interface Code*.

SECTION B104 FIRE-FLOW CALCULATION AREA

B104.1 General. The fire-flow calculation area shall be the total floor area of all floor levels within the *exterior walls*, and under the horizontal projections of the roof of a building, except as modified in Section B104.3.

B104.2 Area separation. Portions of buildings which are separated by *fire walls* without openings, constructed in accordance with the *International Building Code*, are allowed to be considered as separate fire-flow calculation areas.

B104.3 Type IA and Type IB construction. The fire-flow calculation area of buildings constructed of Type IA and Type IB construction shall be the area of the three largest successive floors.

Exception: Fire-flow calculation area for open parking garages shall be determined by the area of the largest floor.

SECTION B105 FIRE-FLOW REQUIREMENTS FOR BUILDINGS

B105.1 One- and two-family dwellings, Group R-3 and R-4 buildings and townhouses. The minimum fire-flow and flow duration requirements for one- and two-family *dwellings*, Group R-3 and R-4 buildings and townhouses shall be as specified in Tables B105.1(1) and B105.1(2).

B105.2 Buildings other than one- and two-family dwellings, Group R-3 and R-4 buildings and townhouses. The minimum fire-flow and flow duration for buildings other than one- and two-family *dwellings*, Group R-3 and R-4 buildings and townhouses shall be as specified in Tables B105.2 and B105.1(2).

TABLE B105.1(1) REQUIRED FIRE-FLOW FOR ONE- AND TWO-FAMILY DWELLINGS, GROUP R-3 AND R-4 BUILDINGS AND TOWNHOUSES

FIRE-FLOW CALCULATION AREA (square feet)	AUTOMATIC SPRINKLER SYSTEM (Design Standard)	MINIMUM FIRE-FLOW (gallons per minute)	FLOW DURATION (hours)	
0-3,600	No automatic sprinkler system	1,000	1	
3,601 and greater	No automatic sprinkler system	Value in Table B105.1(2)	Duration in Table B105.1(2) at the required fire-flow rate	
0-3,600	Section 903.3.1.3 of the <i>International Fire Code</i> or Section P2904 of the <i>International Residential Code</i>	500	1/2	
3,601 and greater	Section 903.3.1.3 of the <i>International Fire Code</i> or Section P2904 of the <i>International Residential Code</i>	1/2 value in Table B105.1(2)	1	

For SI: 1 square foot = 0.0929 m^2 , 1 gallon per minute = 3.785 L/m.

TABLE B105.1(2) REFERENCE TABLE FOR TABLES B105.1(1) AND B105.2

FIRE-FLOW CALCULATION AREA (square feet)					FIRE-FLOW	FLOW DURATION
Type IA and IB ^a	Type IIA and IIIA ^a	Type IV and V-A ^a	Type IIB and IIIB ^a	Type V-B ^a	(gallons per minute)b	(hours)
0-22,700	0-12,700	0-8,200	0-5,900	0-3,600	1,500	
22,701-30,200	12,701-17,000	8,201-10,900	5,901-7,900	3,601-4,800	1,750	
30,201-38,700	17,001-21,800	10,901-12,900	7,901-9,800	4,801-6,200	2,000	2
38,701-48,300	21,801-24,200	12,901-17,400	9,801-12,600	6,201-7,700	2,250	2
48,301-59,000	24,201-33,200	17,401-21,300	12,601-15,400	7,701-9,400	2,500	
59,001-70,900	33,201-39,700	21,301-25,500	15,401-18,400	9,401-11,300	2,750	
70,901-83,700	39,701-47,100	25,501-30,100	18,401-21,800	11,301-13,400	3,000	
83,701-97,700	47,101-54,900	30,101-35,200	21,801-25,900	13,401-15,600	3,250	2
97,701-112,700	54,901-63,400	35,201-40,600	25,901-29,300	15,601-18,000	3,500	3
12,701-128,700	63,401-72,400	40,601-46,400	29,301-33,500	18,001-20,600	3,750	
28,701-145,900	72,401-82,100	46,401-52,500	33,501-37,900	20,601-23,300	4,000	
45,901-164,200	82,101-92,400	52,501-59,100	37,901-42,700	23,301-26,300	4,250	
64,201-183,400	92,401-103,100	59,101-66,000	42,701-47,700	26,301-29,300	4,500	
83,401-203,700	103,101-114,600	66,001-73,300	47,701-53,000	29,301-32,600	4,750	
03,701-225,200	114,601-126,700	73,301-81,100	53,001-58,600	32,601-36,000	5,000	
25,201-247,700	126,701-139,400	81,101-89,200	58,601-65,400	36,001-39,600	5,250	
47,701-271,200	139,401-152,600	89,201-97,700	65,401-70,600	39,601-43,400	5,500	
71,201-295,900	152,601-166,500	97,701-106,500	70,601-77,000	43,401-47,400	5,750	
295,901-Greater	166,501-Greater	106,501-115,800	77,001-83,700	47,401-51,500	6,000	4
_	_	115,801-125,500	83,701-90,600	51,501-55,700	6,250	
_	_	125,501-135,500	90,601-97,900	55,701-60,200	6,500	
_	_	135,501-145,800	97,901-106,800	60,201-64,800	6,750	
_	_	145,801-156,700	106,801-113,200	64,801-69,600	7,000	
_	_	156,701-167,900	113,201-121,300	69,601-74,600	7,250	
_	_	167,901-179,400	121,301-129,600	74,601-79,800	7,500	
_	_	179,401-191,400	129,601-138,300	79,801-85,100	7,750	
_	_	191,401-Greater	138,301-Greater	85,101-Greater	8,000	

For SI: 1 square foot = 0.0929 m^2 , 1 gallon per minute = 3.785 L/m, 1 pound per square inch = 6.895 kPa.

TABLE B105.2 REQUIRED FIRE-FLOW FOR BUILDINGS OTHER THAN ONE- AND TWO-FAMILY DWELLINGS, GROUP R-3 AND R-4 BUILDINGS AND TOWNHOUSES

AUTOMATIC SPRINKLER SYSTEM (Design Standard)	MINIMUM FIRE-FLOW (gallons per minute)	FLOW DURATION (hours)	
No automatic sprinkler system	Value in Table B105.1(2)	Duration in Table B105.1(2)	
Section 903.3.1.1 of the International Fire Code	25% of the value in Table B105.1(2) ^a	Duration in Table B105.1(2) at the reduced flow rate	
Section 903.3.1.2 of the International Fire Code	25% of the value in Table B105.1(2)b	Duration in Table B105.1(2) at the reduced flow rate	

For SI: 1 gallon per minute = 3.785 L/m.

a. Types of construction are based on the International Building Code.

b. Measured at 20 psi residual pressure.

a. The reduced fire-flow shall be not less than 1,000 gallons per minute.

b. The reduced fire-flow shall be not less than 1,500 gallons per minute.

LISTEN DESIGN PLAN BUILD

Preliminary Basis of Design Report **Sewer**

Deer Valley Townhomes

NWC of Miller Road & Deer Valley Road

City of Scottsdale

Maricopa County, Arizona

TSC Project No. 0800

August 2018

Prepared for:

Beardsley 22, Inc 222 W Linger Lane, Phoenix, AZ 85021



1.0 Introduction

The proposed Deer Valley Townhomes development (Project) consists of attached townhomes split between three (3) buildings on a one acre parcel. The Site is defined by the parcel boundary for APN# 212-02-010E and is located at the northwest corner of Miller Road and Deer Valley Road in Scottsdale (see figure 1 below). The current project zoning is PCOC and proposed project zoning is R-3. The site is currently undeveloped and the proposed development will be constructed all at once and will not be phased.

The purpose of this report is to evaluate the existing infrastructure and to determine if the proposed design will adequately support the calculated demands for the proposed developed Site. The Project will be designed and developed in accordance with the 2018 City of Scottsdale Design Standards & Policies Manual (DSPM), County, and State requirements.



Figure 1: Location Map

2.0 Sewer System

The site is a vacant lot with a channel along the east side. There are several existing sewer lines surrounding the property, according to City quarter section maps. Deer Valley Road has an existing 8" VCP sanitary sewer line that flows east to west. An 8" PVC sewer line exists in Miller Road that flows south. An existing sewer line exists in Calistoga Circle with a service stub extends into the Site at the northwest corner. **Appendix A** shows the exact connection location. The proposed sewer system will utilize the existing sewer stub to the property and tie into the main within Calistoga Circle. A 6" PVC sewer line will service the site with 4" laterals to each home.

Based on discussions with the City of Scottsdale, the downstream sewer main and wastewater treatment plant has sufficient capacity to support the Project's sewer proposed flows. The sewer flow from the Project will be conveyed to the City of Scottsdale Wastewater Treatment Plant, 4.2 miles downstream.

3.0 <u>Sewer Analysis</u>

3.1 Jurisdictional Design Criteria

Based on the DSPM all sewer lines shall be designed to provide a minimum peak flow velocity of 2.5 feet per second when flowing completely full and a maximum velocity of 10.0 feet per second. A Manning's roughness coefficient, "n", of 0.013 will be used for all pipe materials. Per MAG Standard Detail 404, the minimum slope requirement for six (6) inch diameter sewer service is 2.08%. Upon completion of the plumbing design in the construction document phase, the service lines to each home or structure will be sized. Cleanouts are located at any direction change greater than 45° or at the end of the line. All buildings are required to have a two-way cleanout at the building per 2015 International Plumbing Code (IPC). Cleanout spacing is equal to or less than 100'.

3.2 Proposed Wastewater Flows

This report supplements preliminary plans proposing 9 residential units. As a result, the final total projected wastewater flow is calculated as follows:

Average Daily Demand =

100 gpcpd

Average Daily Flow (ADF) = 9 DU x 100 gpcpd x 2.5 p/DU = 2,250 gpd

Peak Daily Flow (PDF) = ADF x 4.0 =

9,000 gpd



^{*}ADF based on DSPM section 7-1.403.A

^{*}PDF based on DSPM figure 7-1.2

3.3 Sewer Calculations

Flow capacity per Manning's formula for uniform pipe flow:

$$Q = \frac{1.49}{n} (A) (R_h)^{\frac{2}{3}} (S)^{\frac{1}{2}}$$

Where:

Q = Pipe capacity (cfs)

n = Manning's roughness coefficient

A = Cross sectional area (ft²)
R = Hydraulic radius (ft.)
S = Minimum slope (ft/ft)

Capacity for a full flowing 6" diameter pipe with a minimum slope of 0.0208 ft/ft:

$$\frac{1.49}{0.013}(\pi 0.25^2)(0.13)^{\frac{2}{3}}(0.0208)^{\frac{1}{2}} = 0.81 \ cfs = 523,517 \ gpd$$

9,000 gpd << 523,517 gpd pipe capacity

Flow velocity per Manning's formula for uniform pipe flow:

$$V = \frac{1.49}{n} (R_h)^{\frac{2}{3}} (S)^{\frac{1}{2}}$$

Where:

V = Pipe velocity (ft/s)

n = Manning's roughness coefficient

 $R_h = Hydraulic radius (ft.)$ S = Minimum slope (ft/ft)

The full-flow velocity computed for a 6" sewer line:

$$\frac{1.49}{0.013}(0.13)^{\frac{2}{3}}(0.0208)^{\frac{1}{2}} = 4.12 \, ft/s$$

4.12 fps > 2.5 fps

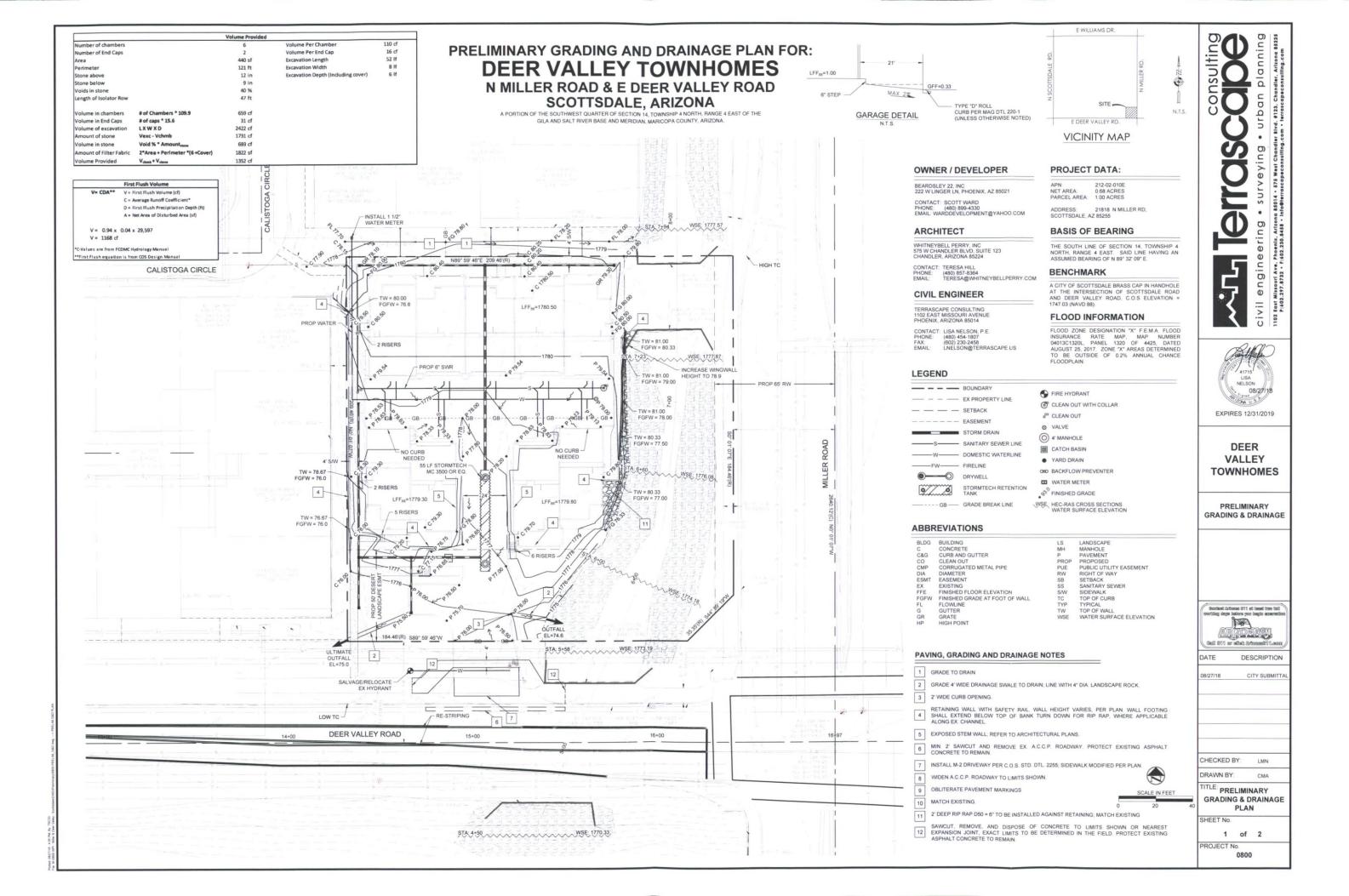
4.0 Conclusion

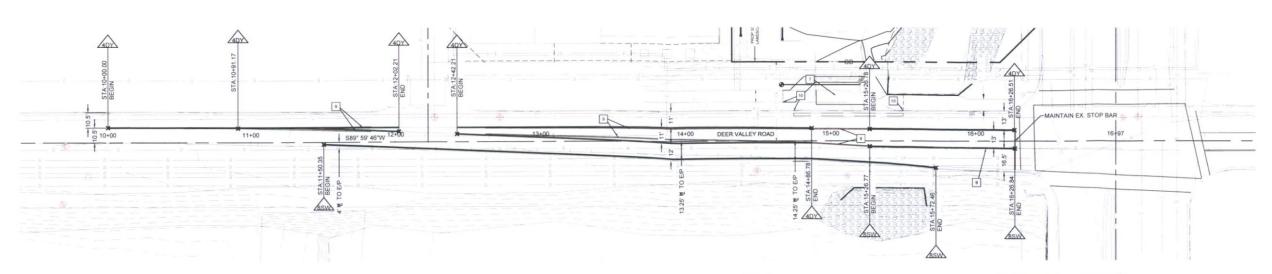
As demonstrated, the proposed sewer system for Deer Valley Townhomes will be in accordance with the 2018 City of Scottsdale Design Standards & Policies Manual and have the capacity to service 9 townhomes on a one acre site. The proposed demand is well under the proposed capacity and an acceptable velocity is obtained.



APPENDIX A

PRELIMINARY GRADING & DRAINAGE PLAN





LEGEND

8" SOLID WHITE LINE 4DY

4" DOUBLE YELLOW LINE

PAVING, GRADING AND DRAINAGE NOTES

GRADE TO DRAIN

GRADE 4' WIDE DRAINAGE SWALE TO DRAIN; LINE WITH 4" DIA. LANDSCAPE ROCK.

3 2' WIDE CURB OPENING.

RETAINING WALL WITH SAFETY RAIL. WALL HEIGHT VARIES, PER PLAN. WALL FOOTING SHALL EXTEND BELOW TOP OF BANK TURN DOWN FOR RIP RAP, WHERE APPLICABLE ALONG EX. CHANNEL.

5 EXPOSED STEM WALL; REFER TO ARCHITECTURAL PLANS.

6 MIN. 2' SAWCUT AND REMOVE EX. A.C.C.P. ROADWAY. PROTECT EXISTING ASPHALT CONCRETE TO REMAIN.

DRIVEWAY PER C.O.S. STD. DTL. 2255; SIDEWALK MODIFIED PER PLAN.

WIDEN A.C.C.P. ROADWAY TO LIMITS SHOWN.

2' DEEP RIP RAP D50 = 6" TO BE INSTALLED AGAINST RETAINING; MATCH EXISTING



consulting

urban planning

Civil engineering • Surveying • Urban planning
1102 East Missoul Ave. Phoents. Arisons \$5014 - 575 West Chondler Bivd. \$123, Chondler, Arisons \$5225
7:402.277,8732 - 7:402.230.8468 - Info@terracepeconsulting.com - terracepeconsulting.com

DEER VALLEY **TOWNHOMES**

PRELIMINARY GRADING & DRAINAGE

Outdood Aufonaue 1911 ed based towe trail tower trail tower trail tower trail to the processor trailing deep balance pron bargin assemblias and trailing tra

DESCRIPTION

CITY SUBMITTA

CHECKED BY:

TITLE: PRELIMINARY
GRADING & DRAINAGE

PLAN SHEET No.

DRAWN BY:

2 of 2

Transportation Impact and Mitigation Analysis (TIMA)

ACCEPTED

CITY OF SCOTTSDALE
TRANSPORTATION DEPARTMENT

DATE: March 31, 2017

REVIEWER: alon Ruck





February 24, 2017

Mr. Michael Sudbeck, PE SP Construction 921 E. Derby Drive Tempe, AZ 85284

RE:

Trip Generation Comparison for a Property Located at 21818 N. Miller Road in Scottsdale, Arizona

Dear Mr. Sudbeck:

This letter is to serve as a trip generation comparison letter concerning a proposed rezoning of a parcel located at the northwest corner of Miller and Deer Valley Roads in Scottsdale, Arizona. This analysis compares the highest trip generation potential of the site under the Existing and Proposed zoning to the planned site development per the City of Scottsdale's *Design Standards and Policies Manual*, a recent email you have provided from Mr. Jesus Murillo, and voice mail received at our office on 2/17/2017 from Mr. Phillip Kercher, both of whom are with the City of Scottsdale.

Proposed Site and Site Characteristics

The subject site is located at the northwest corner of Miller Road and Deer Valley Road consisting of Accessor Parcel Number 212-02-010E, as highlighted in Figure 1. The Maricopa County Assessors website identifies the parcel size at 43,561 square feet (SF). The parcel is currently unimproved, however, a drainage and flood control easement (D&FCE 018365) is located along the east side of the property to direct storm water runoff from north to south with box culverts existing at the northeast and southeast property corners. A 5-foot sidewalk easement also exists at the northwest corner of the site connecting to the adjacent subdivision.

A copy of the proposed site plan layout is provided as an attachment. The site plan shows an improved parcel that includes 11 townhomes with a 24-foot wide right-in/right-out driveway intersecting southbound Miller Road and a full



Figure 1. Vicinity Map

movement 24-foot wide driveway intersecting Deer Valley Road. The Miller Road driveway is located about 240 feet north of the Deer Valley Road centerline (about 205 feet north of the existing Miller Road crosswalk line) and located over an existing box culvert that crosses the adjacent wash. The driveway is currently positioned within the existing southbound to westbound right turn lane taper. The Deer Valley Road

Rezoning Trip Generation Comparison - 21818 N. Miller Road

driveway is located about 225 feet west of the Miller Road centerline (about 175 feet west of the eastbound stop line) and positioned within the eastbound left-turn lane transition taper. Both driveways are located as far away as possible from the existing signal controlled intersection, near the site's north and west property lines.

Existing and Proposed Zoning Characteristics

A change to the underlying zoning for the subject parcel is being requested. From review of the City of Scottsdale's zoning map for the subject parcel, the Existing and Proposed zoning designations are presented below:

- Existing Zoning: PCoP (Planned Convenience Center)
- Proposed Zoning: R-5 (Multi-family Residential)

The City of Scottsdale's Zoning Ordinance provides a Use Table in each zoning designation. The table identifies possible land uses that could be constructed, designated as permitted (P) or conditional use (CU). The following is a selected land use list found under each zoning category. Additional land uses and land use limitations may be associated with the individual land uses, but are not identified in the below listing.

Existing Zoning Land Uses, Selected List (PCoP, Permitted and Conditional Uses)

- Car Wash (CU)
- Courier and Messenger (P)
- Day Care Center within 100 feet of a residential district (CU)
- Dwelling units integrated with business establishments (P)
- Educational Service (P)
- Gas Station (CU)
- Municipal Use (P)
- Office (P)
- Personal Care Service (P)
- Restaurant, excluding drive-through and drive-in restaurants (P)
- Retail (P)
- Veterinary and Pet Care service (P)

Proposed Zoning Land Uses, Selected List (R-5, Permitted and Conditional Uses)

- Day Care Home (P)
- Dwelling, single-family detached or attached (P)
- Dwelling, multi-family (P)
- Municipal Use (P)
- Church (P)
- Day Care Center (CU)
- Orphanage (CU)
- Plant Nursery (CU)
- Public buildings other than hospitals (CU)

When comparing the land uses within each of the two zoning categories, some similar land use types are allowed in both, such as day care center and municipal use. Two of the higher trip generating land uses



Rezoning Trip Generation Comparison - 21818 N. Miller Road

within the Existing zoning category are identified to be a restaurant and gas station, while a day care center (applicable to both zonings) is identified as a one of the highest trip rate generators for the proposed zoning.

In reviewing the City's development standards for each, it appears a maximum non-residential floor area ratio of 0.20 is applicable for building sizes based on the gross lot area, or an estimated 8,000 SF for the subject 1-acre parcel.

Trip Generation Comparison

Trip Generation, Ninth Edition, published by the Institute of Transportation Engineers (ITE) 2012, was used to calculate the maximum trip generation potential for the higher generating land uses in the Existing and Proposed zonings as well as for the proposed 11-unit townhome development for the AM peak hour, PM peak hour, and 24-hour weekday condition. The Trip Generation Manual is the industry standard used by traffic and transportation engineers to provide trip generation characteristics for different types of land uses. The trip generation data provided by ITE is segregated into individual land uses and provides an estimate to the number of trip ends similar land uses would generate. A trip end is defined as one entering or one exiting trip during a designated time period. For the purposes of this analysis, all trip ends are assumed to be made via automobile. Some land uses generate a portion of their business from traffic already on the adjacent roadways, identified as pass-by traffic, and therefore only a percentage of the site's total trips may be new vehicles that were not previously on that roadway. No formal or informal site plans have been developed for the hypothetical land use developments used in the analysis, but are based on engineering judgement. The representative development sizes utilized for the site accounting for some of the restrictions that may exist for the individual land use or associated with the parcel itself.

Table 1 displays the total Weekday, AM peak hour, and PM peak hour trip generation characteristics for the selected land uses. All information is based on ITE's average trip rate data and where applicable, average pass-by trip information as presented in the ITE *Trip Generation Handbook, Second Edition*. The gray shaded land use columns are for the Existing zoning condition, the non-shaded column is the highest trip generating land use identified for the Proposed zoning condition. The blue shaded column is for the planned residential development of the subject parcel with 11 townhomes.

The results indicate that the subject parcel under Existing zoning could generate as many as 140 AM peak hour, 108 PM peak hour, and over 1,300 daily trip ends entering and exiting at the site driveways. Under the Proposed zoning condition, the highest trip generating land use could generate 61 AM peak hour, 62 PM peak hour and 370 daily in/out trips. The planned 11-unit Townhome development for the proposed R-5 zoning is only expected to generate 5 AM and 6 PM peak hour trips and less than 70 total daily trips at the site driveways.



Table 1. Trip Generation Estimate Comparison

	Zoning Condition	Existing - Permitted	Existing - Conditional Use	Proposed - Highest Generator	Proposed - Planned Development
	Land Use	Restaurant	Gas Station	Institutional	Townhouses
_	ITE Land Use Code	939 🗸	946) 945	565 /	230
Description	ITE Land Use Title	Bread/Donut/Bagel Shop without Drive-Through	Gasoline/Service Station w/Convience Market	Day Care Center	Residential Condominium / Townhouse
^	Land Use Variable	1000 SF GFA	Veh. Fueling Positions	1000 SF GFA	Dwelling Units
1	Variable Amount (X)	2	8	5	11
ses	Weekday	N/A	162.78	74.06	5.81
Trip Rates	AM Peak Hour	70.22 🗸	10.16 🗸	12.18	0.44
Į.	PM Peak Hour	28.00 🗸	13.51 🗸	12.34 🗸	0.52 🗸
%	Weekday	50% 🗸	50% ✓	50%	50%
punoqu	AM Peak Hour	47% 🗸	50%	53%	17% 🗸
g	PM Peak Hour	50%	50%	47% /	67% ✓
	Weekday	N/A	1302 🗸	370 🗸	64~
sd	AM Peak Hour Inbound	66 🗸	41 🗸	32 🗸	11/
Fotal Trips	AM Peak Hour Outbound	74 🗸	40 🗸	29 🗸	4
Tot	PM Peak Hour Inbound	28 🗸	54 🗸	29 🗸	4
	PM Peak Hour Outbound	28 🗸	54 🗸	33 🗸	2/
Ji C	AM Peak Hour Pass-by Percentage	49% 🗸	62%	0%	0%
Trafi	PM Peak Hour Pass-by Percentage	50%	56%	0%	0%
Pass-by Traffic	AM Peak Hour Trip Ends	69	50 🗸	0	0
Pa	PM Peak Hour Trip Ends	28 🗸	60 🗸	0	0
	Weekday	N/A	768	(148) 370	64 🗸
s	AM Peak Hour Inbound	32 √	16 🗸	32 🗸	1/
New Trips	AM Peak Hour Outbound	40 🗸	15 🗸	29 🗸	4 🗸
Nev	PM Peak Hour Inbound	14 🗸	24 🗸	29 ✓	4 /
	PM Peak Hour Outbound	14√	24 ✓	33 ✓	2 🗸

Source:



¹ Trip Generation Manual, 9th Ed, ITE, 2012

² Trip Generation Handbook, 2nd Ed., ITE, 2012

Conclusion

In comparing the potential maximum trip generation characteristics under the Existing PCoP zoning and the Proposed R-5 site zoning for this parcel, the existing zoning permits land uses that could generate higher inbound and outbound volumes during daily and peak-hour conditions. The 11 townhomes planned for development under the Proposed zoning is considered a very low traffic generator and will generate significantly less traffic than what is permissible under higher intensity land uses possible under both Existing and Proposed zoning conditions.

If you have any questions or comments, please feel free to contact me at (602) 955-7206.

Respectfully submitted,

Paul Guzek, PE, PTOE Lee Engineering, LLC

attachment



